

EK 307: Electric Circuits

Fall 2017

Lecture 25

Dec 12, 2017

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Administrivia

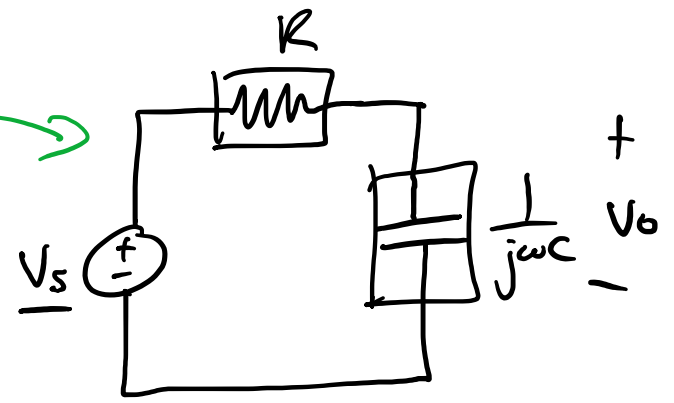
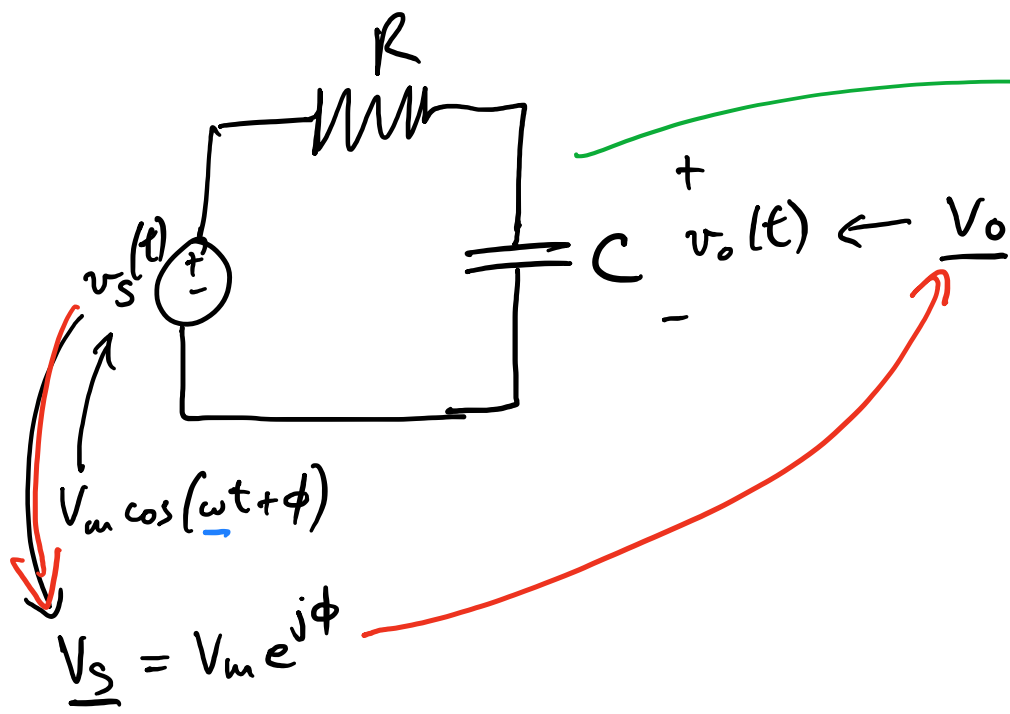
- Homework 9 back, all other homeworks
- HW10/11 = HW10, not graded; do and we go over any questions at review
- Course evaluation
- Review/office hour – doodle poll

Administrivia

- Office hours between now and exam
 - Wed Dec 13 2:30-3:30pm PHO726
 - Thu Dec 14 2:30-3:30pm PHO726
 - Fri Dec 15 2:30-3:30pm PHO726
 - Mon Dec 18 1:30-3:30pm PHO726
 - Tue Dec 19 9:00-10:00am PHO726

Today

- Chapter 14 (14.1-14.4, 14.7)
 - Frequency response and filters
- Course wrap-up



$$|G| = \frac{1}{\sqrt{1 + (\omega RC)^2}}$$

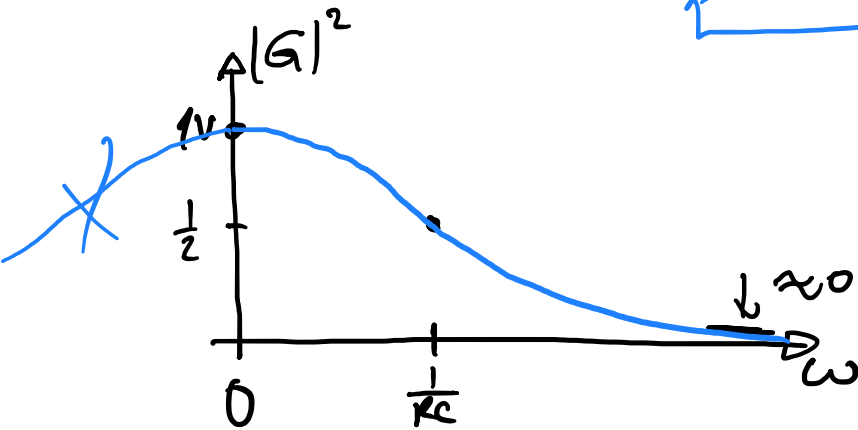
$$|G| = \frac{1}{\sqrt{1 + (\omega RC)^2}}$$

Power gain = $|G|^2 = \frac{1}{1 + (\omega RC)^2}$

Voltage gain:

$$|G| = \sqrt{\frac{1}{1^2 + (\omega RC)^2}}$$

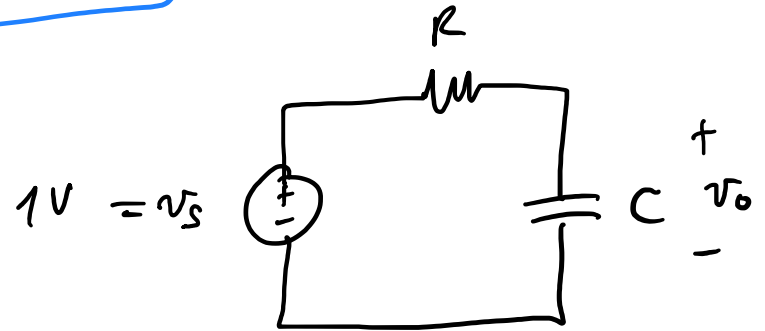
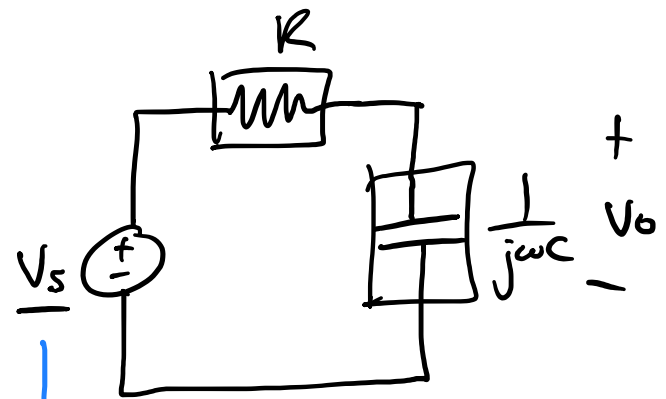
Power gain = $|G|^2 = \frac{1}{1 + (\omega RC)^2}$



For $\omega = 0$: $|G|^2 = 1$

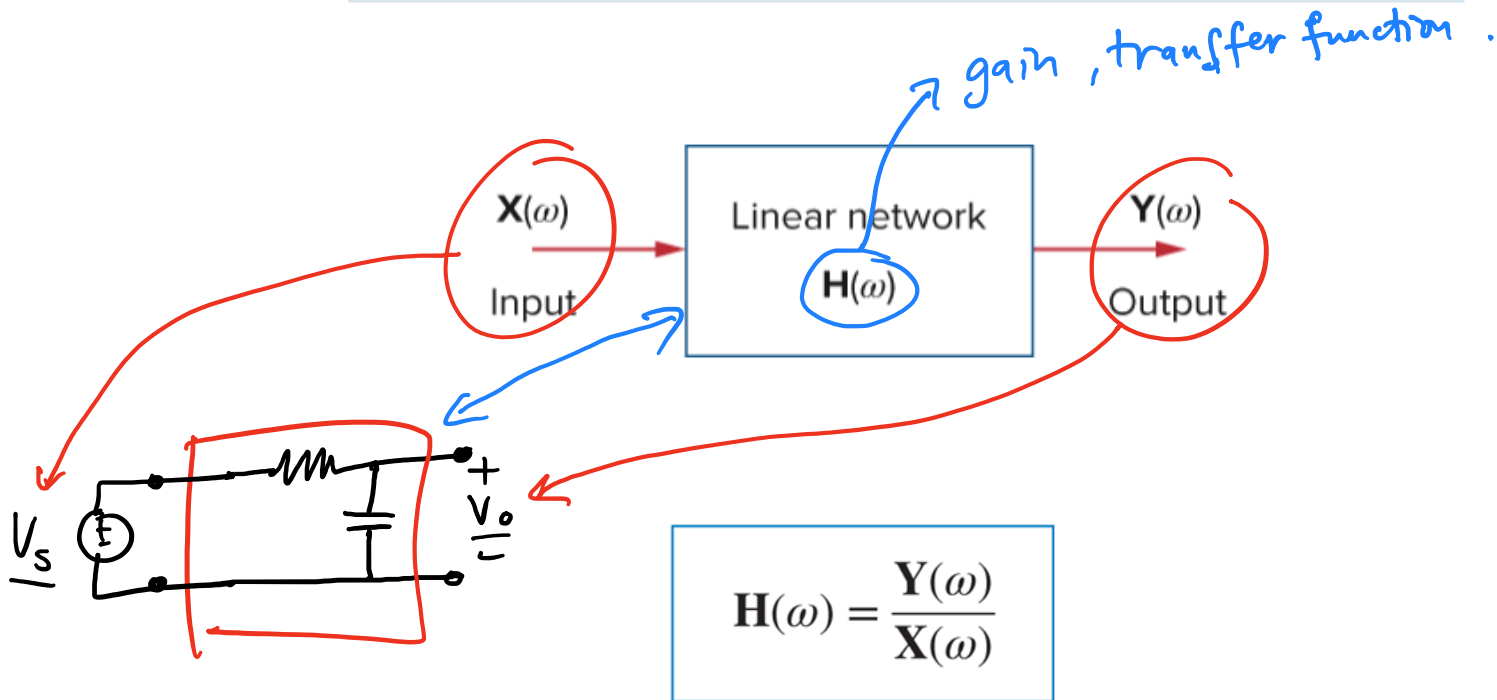
$\omega \Rightarrow \infty$: $|G|^2 = \frac{1}{1 + (\omega RC)^2} \approx \frac{1}{(\omega RC)^2} \rightarrow 0$

$\omega = \frac{1}{RC}$: $|G|^2 = \frac{1}{2}$



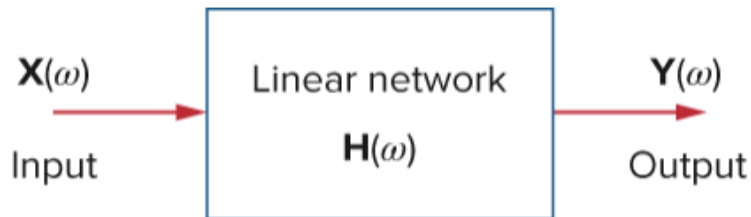
Chapter 14: Frequency Response

The **frequency response** of a circuit is the variation in its behavior with change in signal frequency.



Chapter 14: Frequency Response

The **frequency response** of a circuit is the variation in its behavior with change in signal frequency.



$$H(\omega) = \frac{Y(\omega)}{X(\omega)}$$

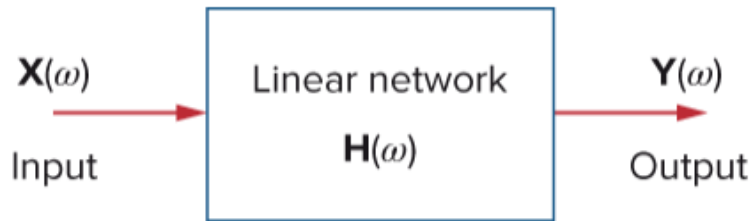
$$H(\omega) = \text{Voltage gain} = \frac{V_o(\omega)}{V_i(\omega)}$$

$$H(\omega) = \text{Current gain} = \frac{I_o(\omega)}{I_i(\omega)}$$

$$H(\omega) = \text{Transfer impedance} = \frac{V_o(\omega)}{I_i(\omega)}$$

$$H(\omega) = \text{Transfer admittance} = \frac{I_o(\omega)}{V_i(\omega)}$$

Chapter 14: Frequency Response



$$\bar{H}(\omega) = H(\omega) / \angle \phi.$$

$$H(\omega) = \frac{N(\omega)}{D(\omega)}$$

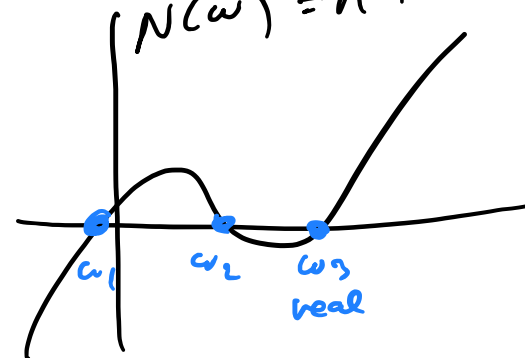
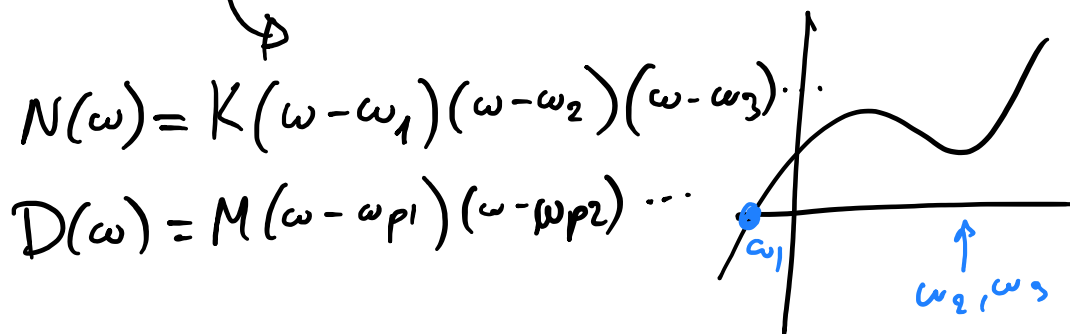
zeros of transfer fun

poles of trans fun

$$N(\omega) = A + B\omega + C\omega^2 + D\omega^3 + \dots$$

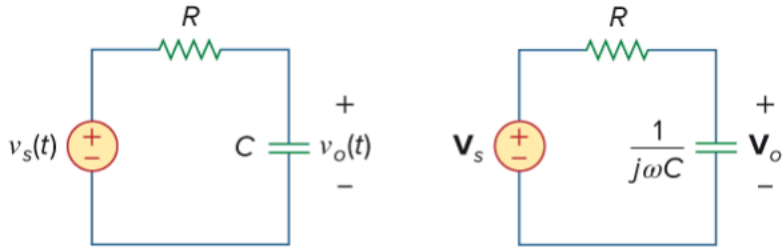
ω^n (for N cat elements)

$$N(\omega) = A + B\omega + C\omega^2 + D\omega^3$$



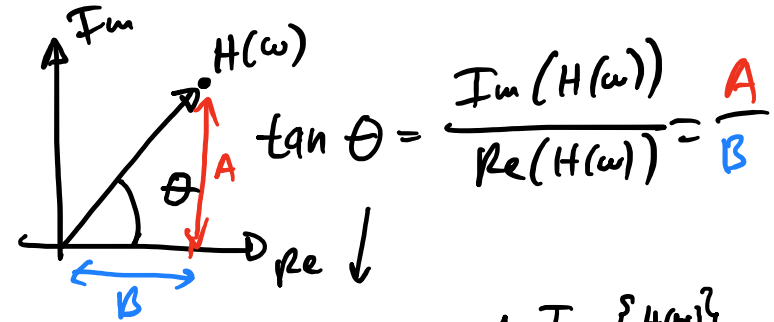
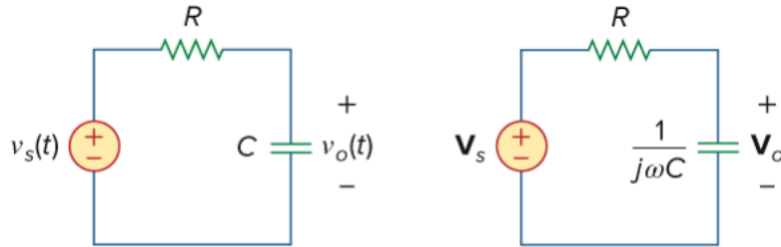
Example 14.1

For the RC circuit in [Fig. 14.2\(a\)](#), obtain the transfer function $\mathbf{V}_o/\mathbf{V}_s$ and its frequency response. Let $v_s = V_m \cos \omega t$.



Example 14.1

For the RC circuit in Fig. 14.2(a), obtain the transfer function V_o/V_s and its frequency response. Let $v_s = V_m \cos \omega t$.

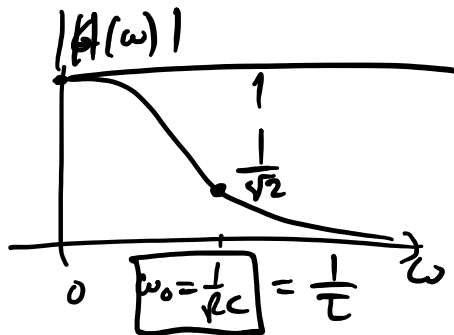


Phase response: $\theta(\omega) = \tan^{-1} \frac{\text{Im}\{H(\omega)\}}{\text{Re}\{H(\omega)\}}$

$$H(\omega) = \frac{V_o}{V_s} = \frac{1/j\omega C}{R + 1/j\omega C} = \frac{1}{1 + j\omega RC}$$

$$\sqrt{H(\omega) H^*(\omega)}$$

Magnitude response:



$$H = \frac{1}{\sqrt{1 + (\omega/\omega_0)^2}}$$

Corner frequency

$$\omega_0 = \frac{1}{RC}$$

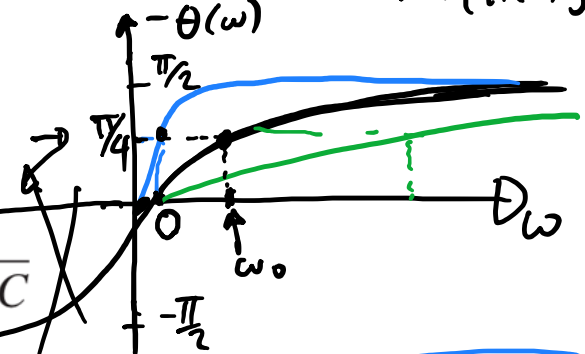
$$H(\omega) = \frac{1 - j\omega RC}{1 + (\omega RC)^2} = \frac{1}{1 + (\omega RC)^2} - j \frac{\omega RC}{1 + (\omega RC)^2}$$

$$\phi = -\tan^{-1} \frac{\omega}{\omega_0}$$

$$\theta(\omega) = \tan^{-1} \frac{-\omega RC / 0}{1/0}$$

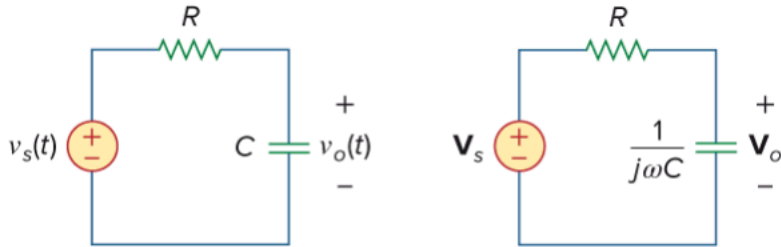
$$= -\tan^{-1} \omega RC$$

$$\theta(\omega) = -\tan^{-1} \omega / \omega_0$$



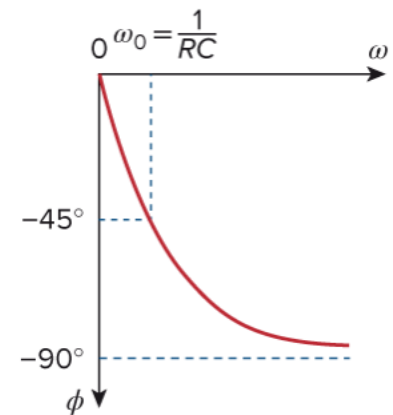
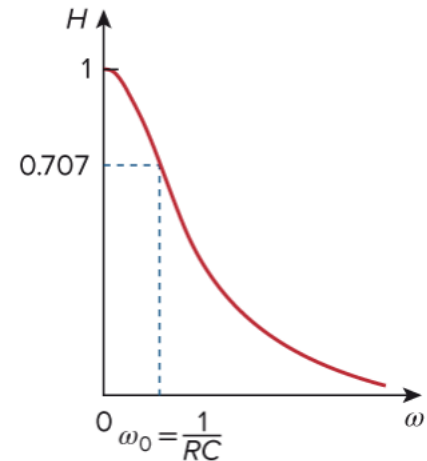
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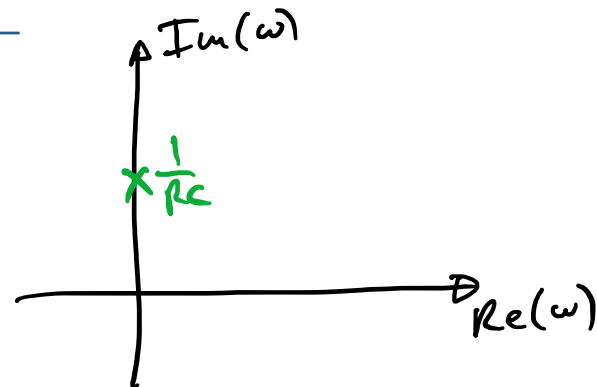
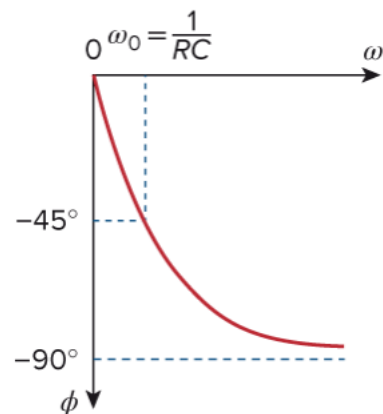
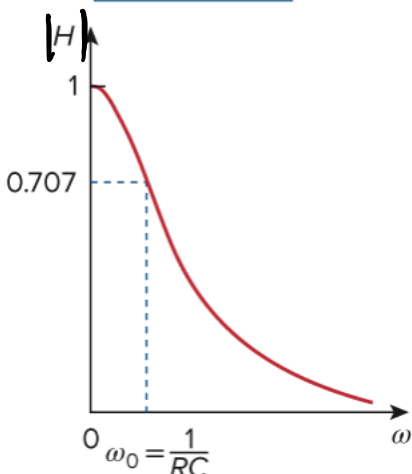
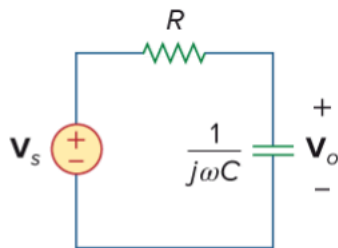
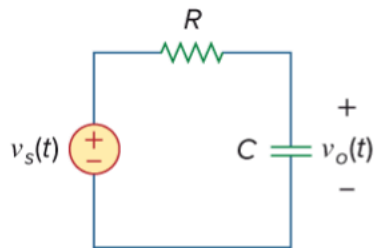
$$\mathbf{H}(\omega) = \frac{\mathbf{V}_o}{\mathbf{V}_s} = \frac{1/j\omega C}{R + 1/j\omega C} = \frac{1}{1 + j\omega RC}$$

$$H = \frac{1}{\sqrt{1 + (\omega/\omega_0)^2}}, \quad \phi = -\tan^{-1} \frac{\omega}{\omega_0}$$



Example 14.1

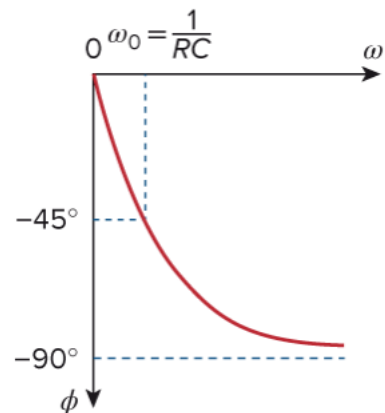
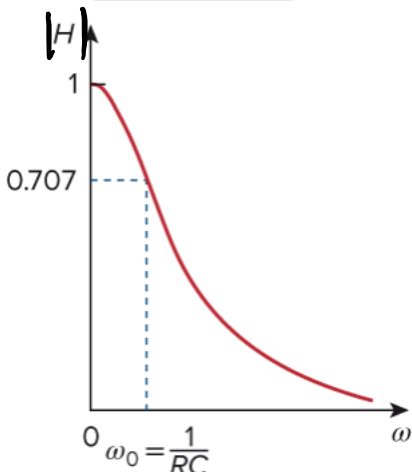
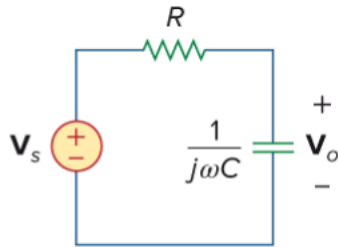
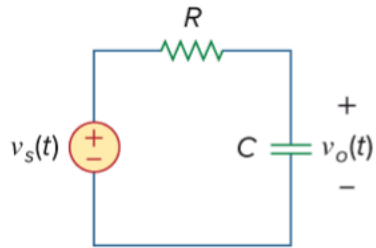
For the RC circuit in Fig. 14.2(a), obtain the transfer function V_o/V_s and its frequency response. Let $v_s = V_m \cos \omega t$.



$$\begin{aligned}
 H(\omega) &= \frac{1}{1 + j\omega RC} = \frac{A (\cancel{\omega - \omega_{z1}}) (\cancel{\omega - \omega_{z2}}) \dots}{(\omega - \omega_{p1}) (\cancel{\omega - \omega_{p2}}) \dots} \\
 &= \frac{\frac{1}{jRC}}{\frac{1}{jRC} + \omega} = \frac{\frac{1}{jRC}}{\omega - \frac{-1}{jRC}} \\
 &= \frac{\boxed{\frac{1}{jRC}} \rightarrow A}{\omega - \underbrace{\boxed{j \frac{1}{RC}}}_{\substack{\rightarrow \omega_0 \\ \rightarrow j \frac{1}{RC}}} }
 \end{aligned}$$

Example 14.1

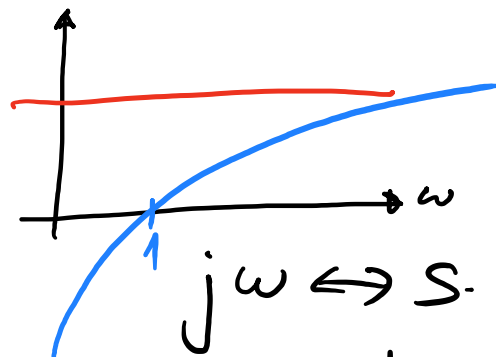
For the RC circuit in Fig. 14.2(a), obtain the transfer function V_o/V_s and its frequency response. Let $v_s = V_m \cos \omega t$.



$$H(\omega) = \frac{1}{1 + j\omega RC} = \frac{\text{const}}{\text{line}}$$

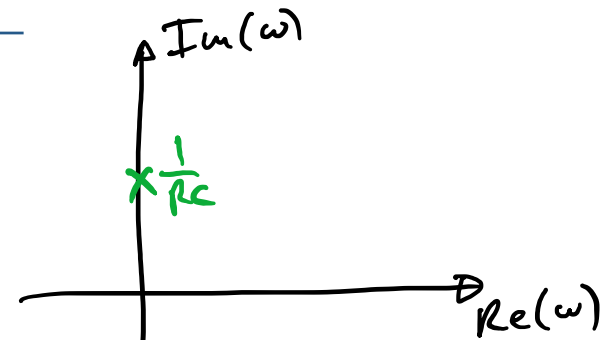
$$H(\omega) = \frac{1}{1 + j\omega RC} = \frac{A(\omega - \omega_{z1})(\omega - \omega_{z2}) \dots}{(\omega - \omega_{p1})(\omega - \omega_{p2}) \dots} = \frac{A \cdot B \cdot C}{D \cdot E}$$

$$\ln H(\omega) = \ln\left(\frac{A \cdot B \cdot C}{D \cdot E}\right) = \ln A + \ln B + \ln C - \ln D - \ln E$$



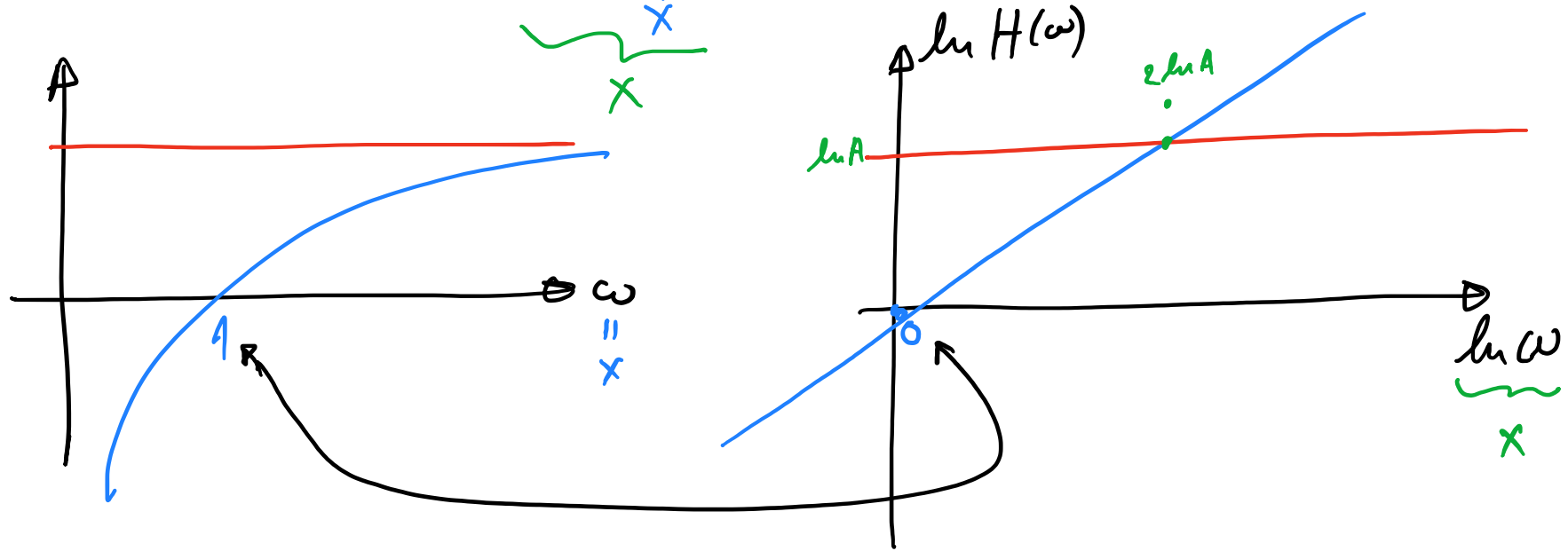
$$H(\omega) = \frac{1}{1 + sRC}$$

$$\rightarrow s = \frac{-1}{RC}$$



$$= \boxed{\ln A} - \boxed{\ln(\omega - \omega_{p1})}$$

$$\ln H(\omega) = \boxed{\ln A} + \boxed{\ln(\omega)}$$



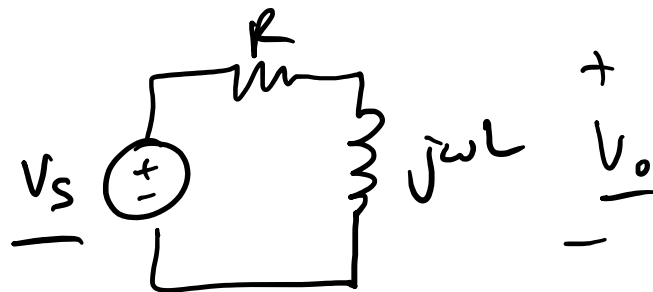
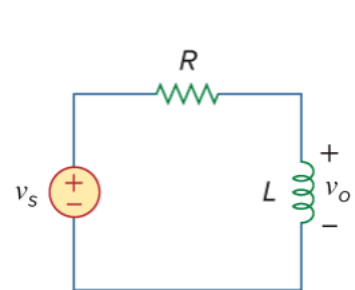
$$H(\omega) = \frac{1}{1 + j\omega RC}$$

$$\begin{aligned} \ln |H(\omega)| &= \ln \frac{1}{\sqrt{1 + (\omega RC)^2}} = \ln \left(\frac{1}{[1 + (\omega RC)^2]} \right)^{\frac{1}{2}} = \frac{1}{2} \ln \frac{1}{1 + (\omega RC)^2} \\ &= \frac{1}{2} [\cancel{\ln 1} - \ln(1 + (\omega RC)^2)] = -\frac{1}{2} \ln(1 + (\omega RC)^2) \\ &= -\frac{1}{2} \ln(1 + (e^{\ln \omega} RC)^2) \\ &= -\frac{1}{2} \ln(\omega RC)^2 = -\ln \omega RC \end{aligned}$$

A small diagram on the left shows a circle with a horizontal axis labeled $\ln \omega$ and a vertical axis. A green line passes through the origin, and a red line is tangent to the circle at the origin. A green dot is marked on the horizontal axis at $\frac{1}{RC}$.

Practice Problem 14.1

Obtain the transfer function $\mathbf{V}_o/\mathbf{V}_s$ of the RL circuit in Fig. 14.4, assuming $v_s = V_m \cos \omega t$. Sketch its frequency response.



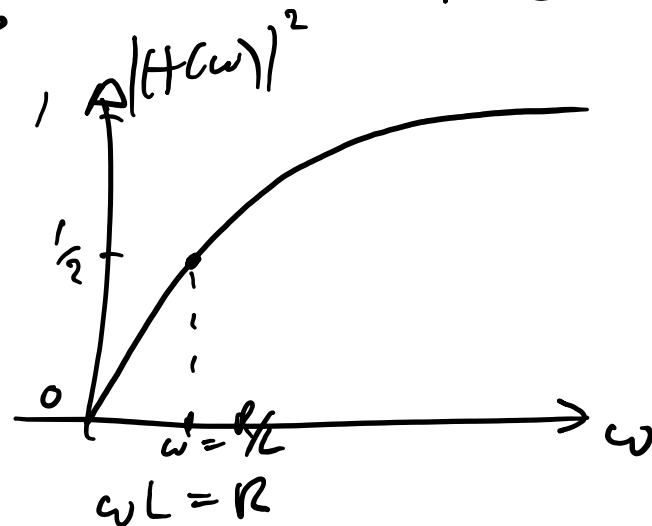
$$\underline{V_o} = \frac{j\omega L}{R + j\omega L} \underline{V_s} = \frac{j\omega/\omega_z}{1 + j\omega/\omega_p} \rightarrow |H(\omega)|^2 = \frac{(\omega L)^2}{R^2 + (\omega L)^2}$$

$\omega = 0 \rightarrow 0$
 $\omega = \infty \rightarrow 1$

Zeros: $\omega_z = 0$

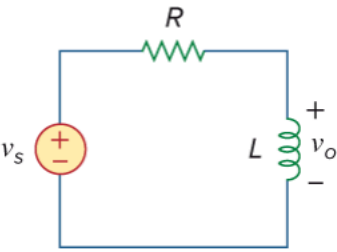
Poles: $j\omega = -\frac{R}{L}$

$$\omega_p = \frac{R}{L} = \frac{1}{\tau}$$



Practice Problem 14.1

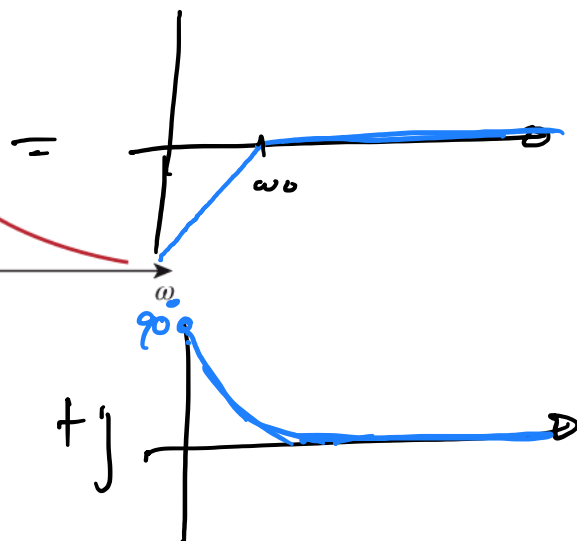
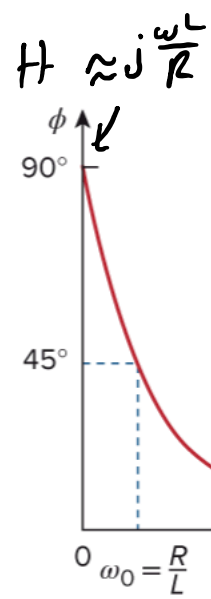
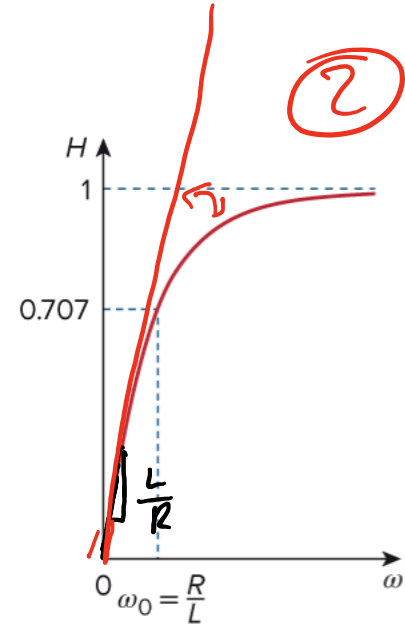
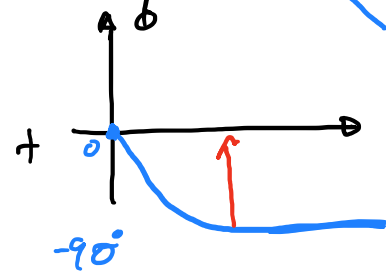
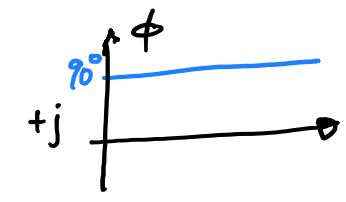
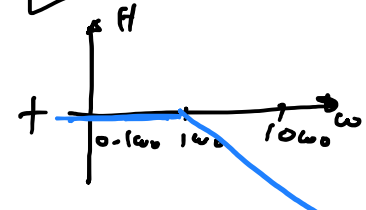
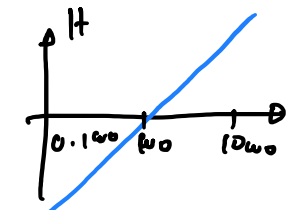
Obtain the transfer function V_o/V_s of the RL circuit in Fig. 14.4, assuming $v_s = V_m \cos \omega t$. Sketch its frequency response.



$$\frac{V_o}{V_s} = \frac{j\omega L}{R + j\omega L} = \frac{j\omega L/R}{1 + j\omega L/R} = \frac{j\omega/\omega_0}{1 + j\omega/\omega_0}$$

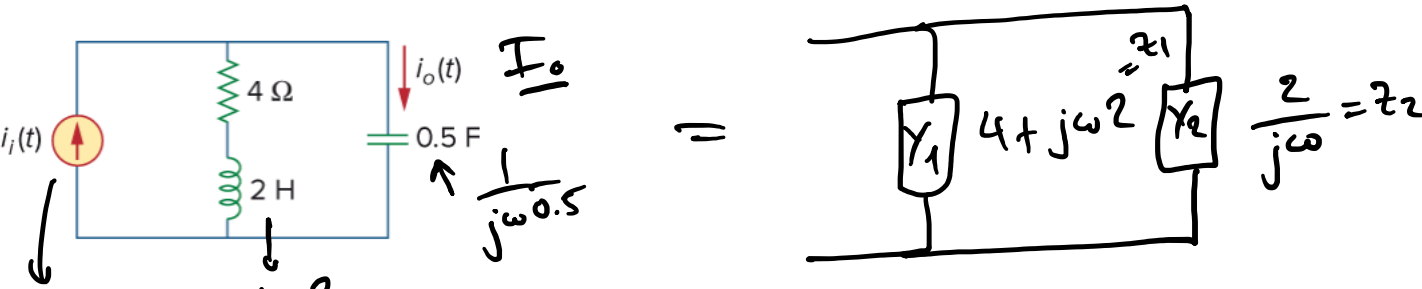
$\omega_0 = R/L$

① $H_{dB} = 20 \log_{10} \frac{V_o}{V_s} =$



Example 14.2

For the circuit in Fig. 14.6, calculate the gain $\underline{I}_o(\omega)/\underline{I}_i(\omega)$ and its poles and zeros.



The circuit diagram shows an input current $\underline{I}_i$ entering a node. This node is connected to a $4\ \Omega$ resistor and a 2 H inductor in parallel. The output current $\underline{I}_o$ is the current flowing into a 0.5 F capacitor. The admittance of the inductor is $j\omega 2$. The admittance of the capacitor is $\frac{1}{j\omega 0.5}$.

The equivalent circuit is shown as a parallel combination of three admittances: Y_1 (the $4\ \Omega$ resistor), $4 + j\omega 2$ (the inductor's admittance), and Y_2 (the capacitor's admittance). The relationship $\frac{2}{j\omega} = Z_2$ is noted, where Z_2 is the impedance of the capacitor.

Handwritten calculations for the gain:

$$\underline{I}_o = \frac{j\omega/2}{j\omega/2 + \frac{1}{4 + j\omega 2}} \underline{I}_i = \frac{1}{Y_1 + Y_2}$$

$$= \frac{j\frac{\omega}{2}(4 + j\omega 2)}{j\frac{\omega}{2}(4 + j\omega 2) + 1} = \frac{1}{j\omega 2 + (j\omega)^2 + 1}$$

Substituting $s \leftarrow j\omega$:

$$= \frac{2s + s^2}{2s + s^2 + 1} = \frac{s(s+2)}{(s+1)^2}$$

Annotations for poles and zeros:

- zeros: $s=0, s=-2$
- poles: $s=-1$

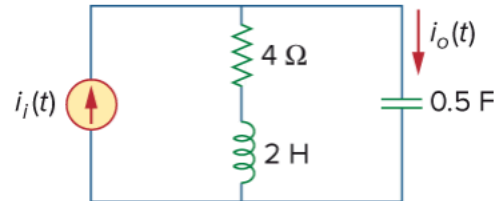
Additional handwritten notes on the right:

$$Y_1 = \frac{1}{Z_1}$$

$$Y_2 = \frac{1}{Z_2}$$

Example 14.2

For the circuit in **Fig. 14.6**, calculate the gain $\mathbf{I}_o(\omega)/\mathbf{I}_i(\omega)$ and its poles and zeros.



$$\mathbf{I}_o(\omega) = \frac{4 + j2\omega}{4 + j2\omega + 1/j0.5\omega} \mathbf{I}_i(\omega)$$

$$\frac{\mathbf{I}_o(\omega)}{\mathbf{I}_i(\omega)} = \frac{j0.5\omega(4 + j2\omega)}{1 + j2\omega + (j\omega)^2} = \frac{s(s + 2)}{s^2 + 2s + 1}, \quad s = j\omega$$

The zeros are at

$$s(s + 2) = 0 \quad \Rightarrow \quad z_1 = 0, z_2 = -2$$

The poles are at

$$s^2 + 2s + 1 = (s + 1)^2 = 0$$

Bode Plots

$$G_{\text{B}} = \text{Number of bels} = \log_{10} \frac{P_2}{P_1} = \log |G|^2$$

Gain in decibels (dB):

$$G_{\text{dB}} = 10 \log_{10} \frac{P_2}{P_1} = 10 \log_{10} \frac{V_2^2 / R}{V_1^2 / R} = 10 \log_{10} \left(\frac{V_2}{V_1} \right)^2$$

$$G_{\text{dB}} = 20 \log_{10} \frac{V_2}{V_1}$$

Bode Plots

$$G = \text{Number of bels} = \log_{10} \frac{P_2}{P_1}$$

Gain in decibels (dB):

$$G_{\text{dB}} = 10 \log_{10} \frac{P_2}{P_1}$$

$$G_{\text{dB}} = 20 \log_{10} \frac{V_2}{V_1}$$

$$G_{\text{dB}} = 20 \log_{10} \frac{I_2}{I_1}$$

Bode Plots

$$\mathbf{H} = H/\underline{\phi} = He^{j\phi}$$

$$\ln \mathbf{H} = \ln H + \ln e^{j\phi} = \ln H + j\phi$$

$$H_{\text{dB}} = 20 \log_{10} H$$

Bode Plots

$$\mathbf{H} = H/\phi = He^{j\phi}$$

$$\ln \mathbf{H} = \ln H + \ln e^{j\phi} = \ln H + j\phi$$

$$H_{\text{dB}} = 20 \log_{10} H$$

Magnitude H	$20 \log_{10} H(\text{dB})$
0.001	-60
0.01	-40
0.1	-20
0.5	-6
$1/\sqrt{2}$	-3
1	0
$\sqrt{2}$	3
2	6
10	20
20	26
100	40
1000	60

Bode Plots: Adding on Log Scale

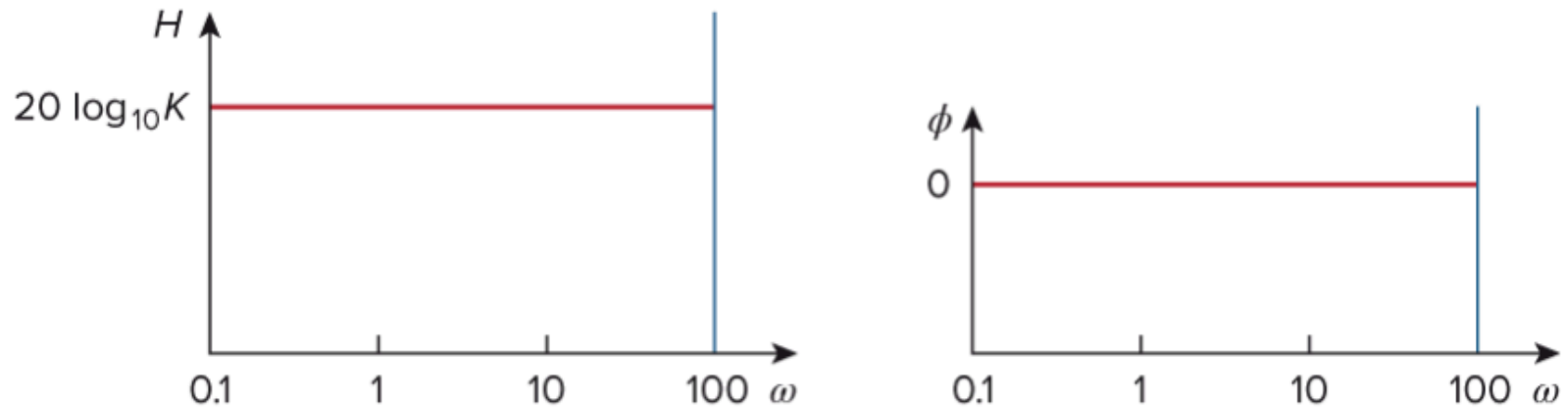
$$\mathbf{H}(\omega) = \frac{K(j\omega)^{\pm 1}(1 + j\omega/z_1)[1 + j2\zeta_1\omega/\omega_k + (j\omega/\omega_k)^2]\cdots}{(1 + j\omega/p_1)[1 + j2\zeta_2\omega/\omega_n + (j\omega/\omega_n)^2]\cdots} \quad (14.15)$$

$$= \frac{K s (1 + s/z_1) [1 + \zeta_1 s/\omega_k + (s/\omega_k)^2]}{\dots}$$

1. A gain K
2. A pole $(j\omega)^{-1}$ or zero $(j\omega)$ at the origin
3. A simple pole $1/(1 + j\omega/p_1)$ or zero $(1 + j\omega/z_1)$
4. A quadratic pole $1/[1 + j2\zeta_2\omega/\omega_n + (j\omega/\omega_n)^2]$ or zero $[1 + j2\zeta_1\omega/\omega_k + (j\omega/\omega_k)^2]$

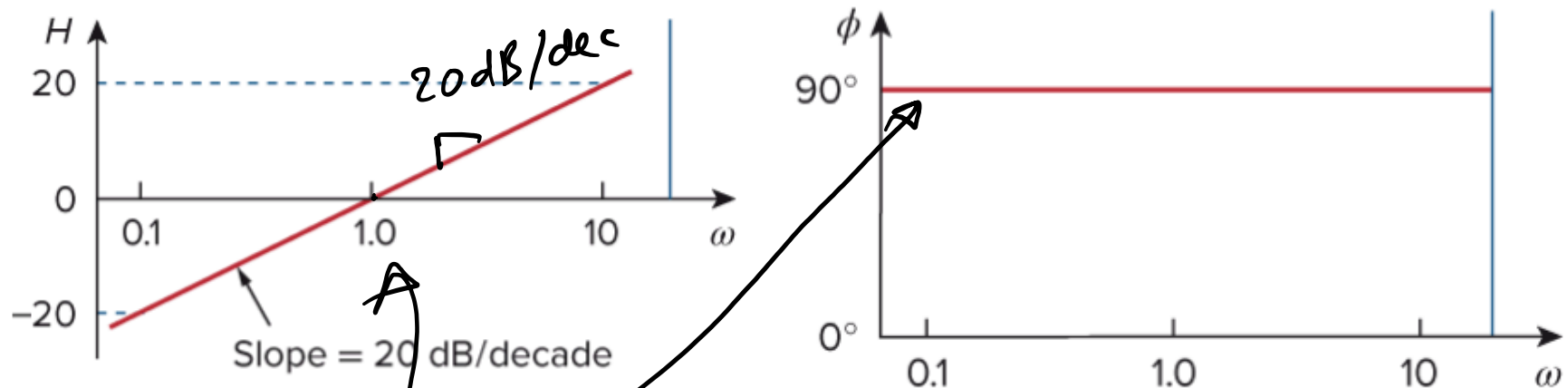
Bode Plots: A constant term

Constant term: For the gain K , the magnitude is $20 \log_{10} K$ and the phase is 0° ; both are constant with frequency. Thus, the magnitude and phase plots of the gain are shown in **Fig. 14.9**. If K is negative, the magnitude remains $20 \log_{10} |K|$ but the phase is $\pm 180^\circ$.



Bode Plots: Linear terms

Pole/zero at the origin: For the zero ($j\omega$) at the origin, the magnitude is $20 \log_{10}\omega$ and the phase is 90° . These are plotted in [Fig. 14.10](#), where we notice that the slope of the magnitude plot is 20 dB/decade, while the phase is constant with frequency.



$$H(\omega) = A j\omega$$

$$20 \log_{10} H(\omega) = 20 \log_{10} A + 20 \log_{10} (j\omega)$$

Bode Plots: Linear terms away from zero frequency

$$H(\omega) = \frac{A(\omega - \omega_1) \left(\frac{j\omega}{\omega_1} - 1 \right)}{\left(1 + \frac{j\omega}{z_1} \right) \left(1 + \frac{j\omega}{z_2} \right) \dots}$$

$$H_{dB} = 20 \log_{10} \left| 1 + \frac{j\omega}{z_1} \right| \Rightarrow 20 \log_{10} 1 = 0$$

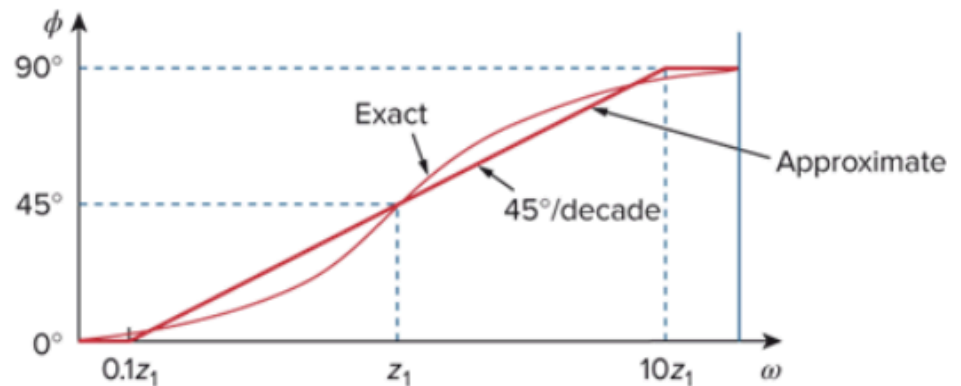
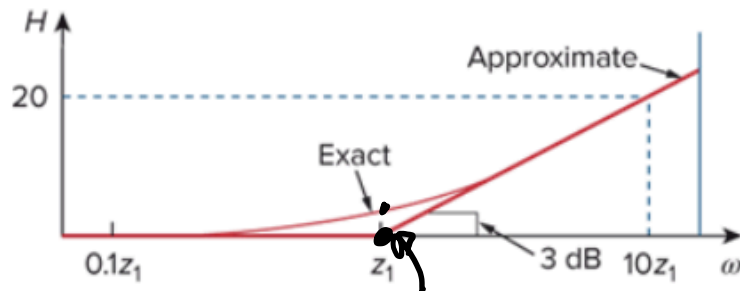
as $\omega \rightarrow 0$

$$H_{dB} = 20 \log_{10} \left| 1 + \frac{j\omega}{z_1} \right| \Rightarrow 20 \log_{10} \frac{\omega}{z_1}$$

as $\omega \rightarrow \infty$

$$\omega = z_1 \Rightarrow \left| 1 + j \frac{\omega}{z_1} \right| = |1 + j1| = \sqrt{2} = H$$

$$20 \log_{10} |(1 + j1)| = 20 \log_{10} \sqrt{2} \simeq 3 \text{ dB}$$



Bode Plots: Quadratic Term

Quadratic pole/zero: The magnitude of the quadratic pole $1/[1 + j2\zeta_2\omega/\omega_n + (j\omega/\omega_n)^2]$ is $-20 \log_{10}|1 + j2\zeta_2\omega/\omega_n + (j\omega/\omega_n)^2|$ and the phase is $-\tan^{-1}(2\zeta_2\omega/\omega_n)/(1 - \omega^2/\omega_n^2)$. But

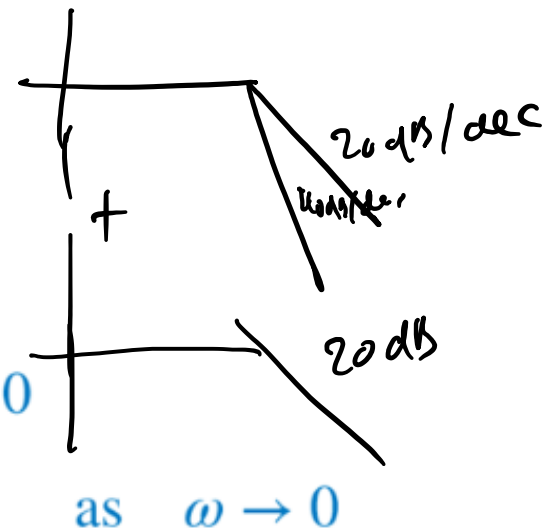
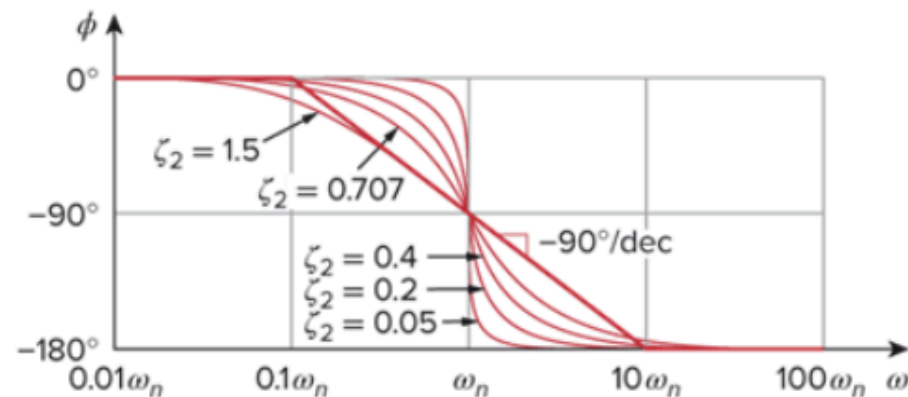
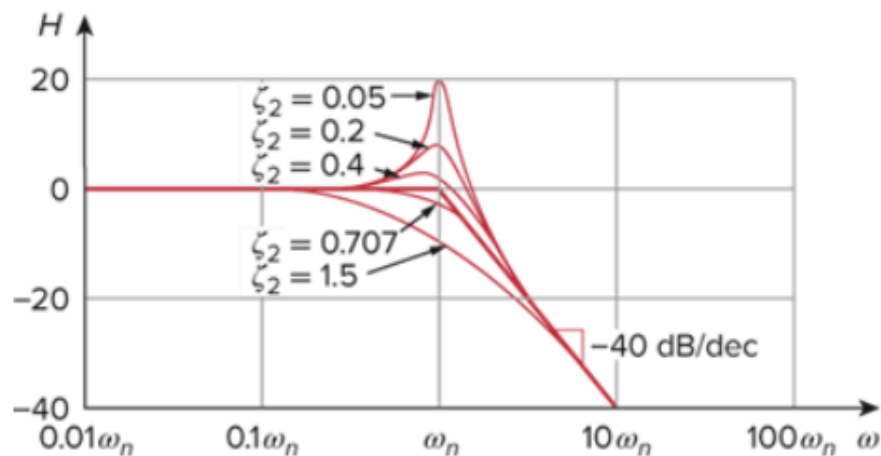
$$H(\omega) = \frac{(j\omega)(j\omega)}{1 + j2\zeta_2\omega/\omega_n + (j\omega/\omega_n)^2}$$

$$H_{dB} = -20 \log_{10} \left| 1 + \frac{j2\zeta_2\omega}{\omega_n} + \left(\frac{j\omega}{\omega_n} \right)^2 \right| \Rightarrow 0$$

as $\omega \rightarrow 0$

$$H_{dB} = -20 \log_{10} \left| 1 + \frac{j2\zeta_2\omega}{\omega_n} + \left(\frac{j\omega}{\omega_n} \right)^2 \right| \Rightarrow -40 \log_{10} \frac{\omega}{\omega_n}$$

as $\omega \rightarrow \infty$



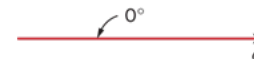
Factor

Magnitude

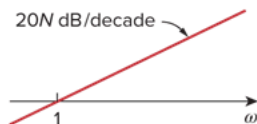
Phase

$$20 \log_{10} K$$

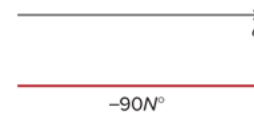
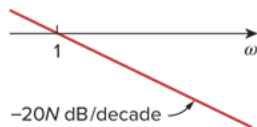
K



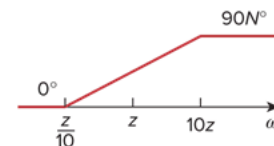
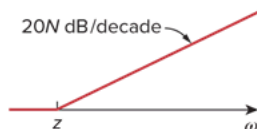
$(j\omega)^N$



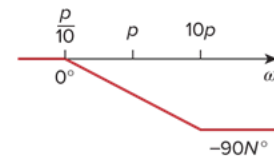
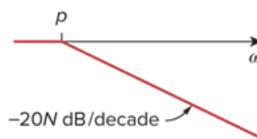
$\frac{1}{(j\omega)^N}$



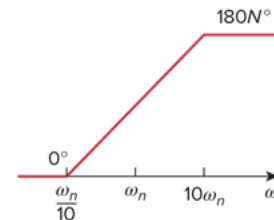
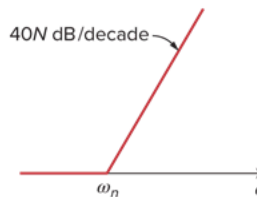
$\left(\frac{1+j\omega}{z}\right)^N$



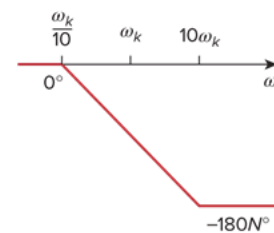
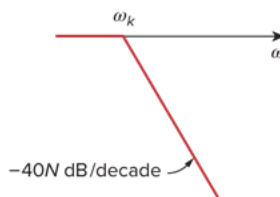
$\frac{1}{(1+j\omega/p)^N}$



$\left[1 + \frac{2j\omega\zeta}{\omega_n} + \left(\frac{j\omega}{\omega_n}\right)^2\right]^N$



$\frac{1}{[1 + 2j\omega\zeta/\omega_k + (j\omega/\omega_k)^2]^N}$



Practice Problem 14.3

Draw the Bode plots for the transfer function

$$H(\omega) = \frac{5(j\omega + 2)}{j\omega(j\omega + 10)}$$

$$= \frac{10(1 + j\frac{\omega}{2})}{j\omega(1 + j\frac{\omega}{10})}$$

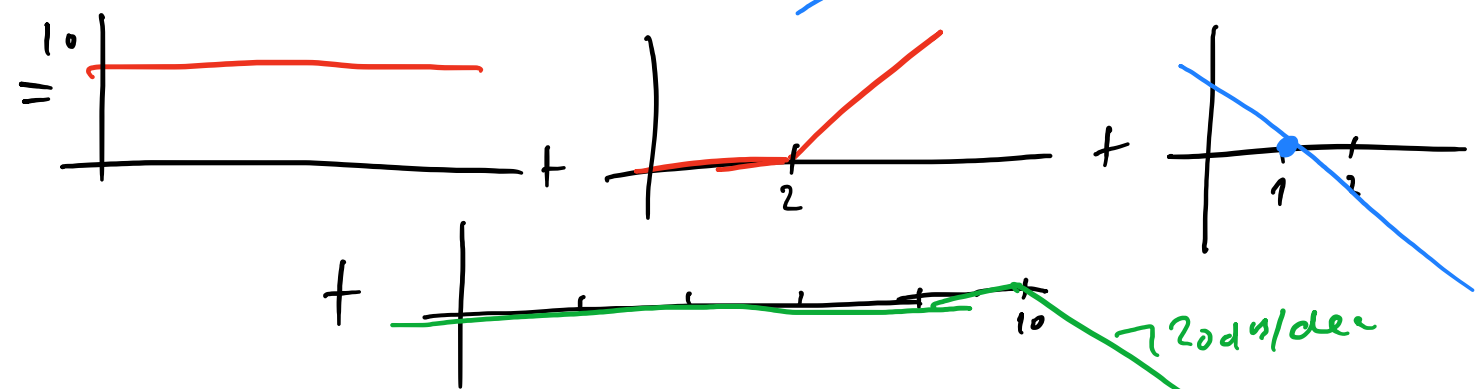
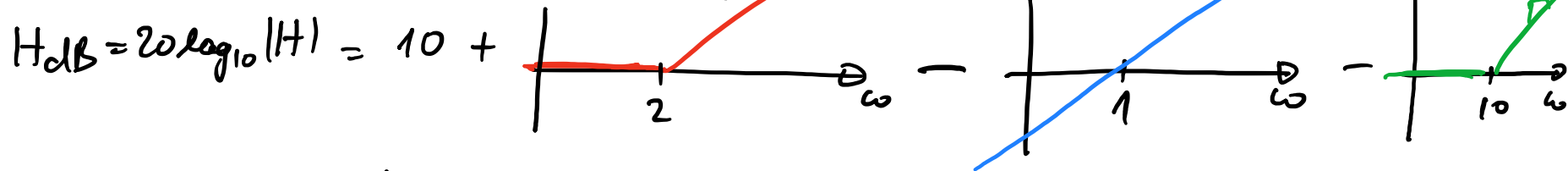
$$= \frac{10(1 + j\frac{\omega}{2})}{j\omega(1 + j\frac{\omega}{10})}$$

$$A \left(1 + \frac{j\omega}{z_1} \right)$$

$\omega_{z_1} \left(\frac{1}{z_1} \right)$

$$j\omega \left(1 + \frac{j\omega}{p_1} \right)$$

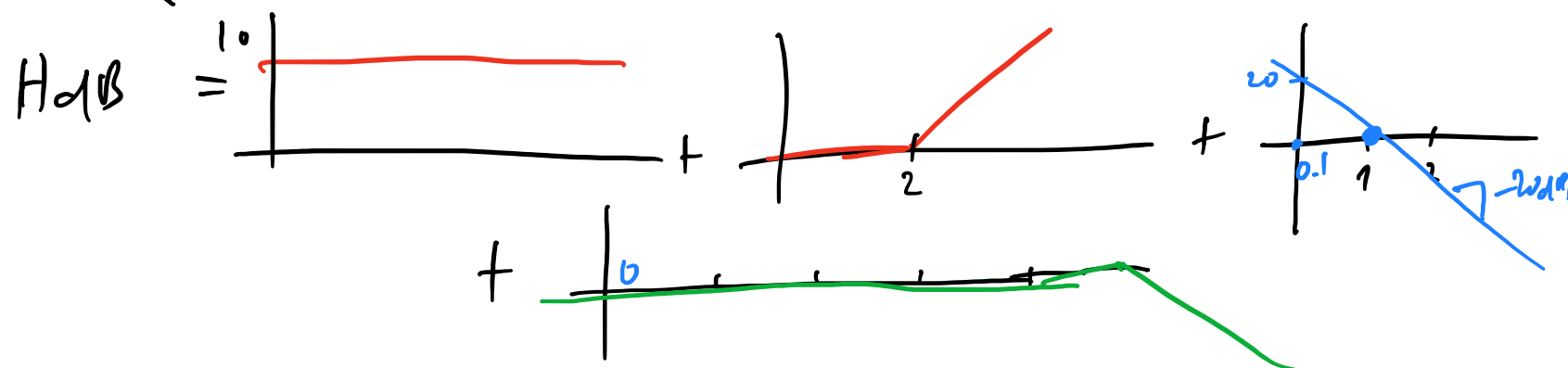
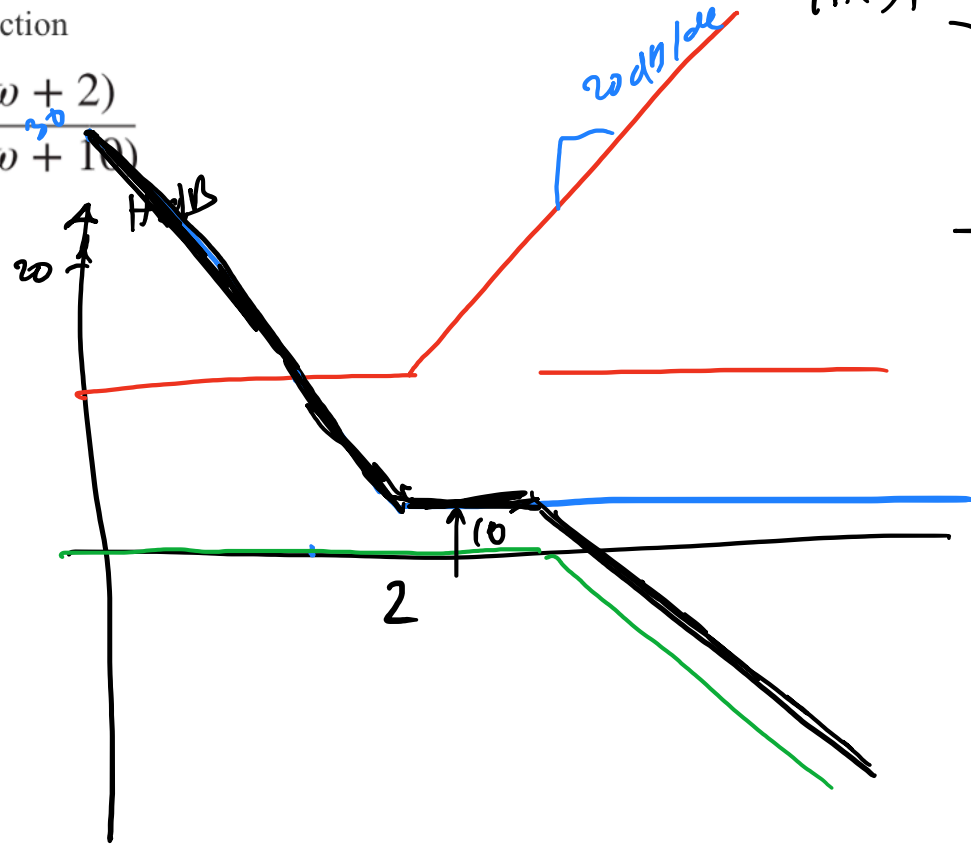
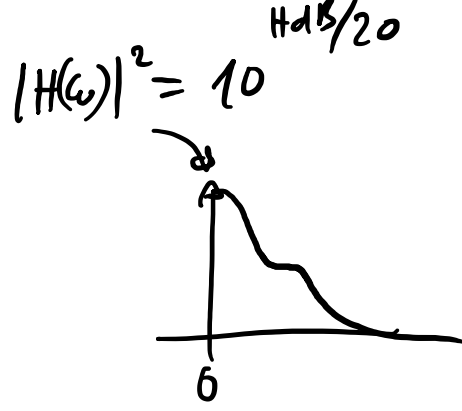
$\omega_{p_1} \left(\frac{1}{p_1} \right)$



Practice Problem 14.3

Draw the Bode plots for the transfer function

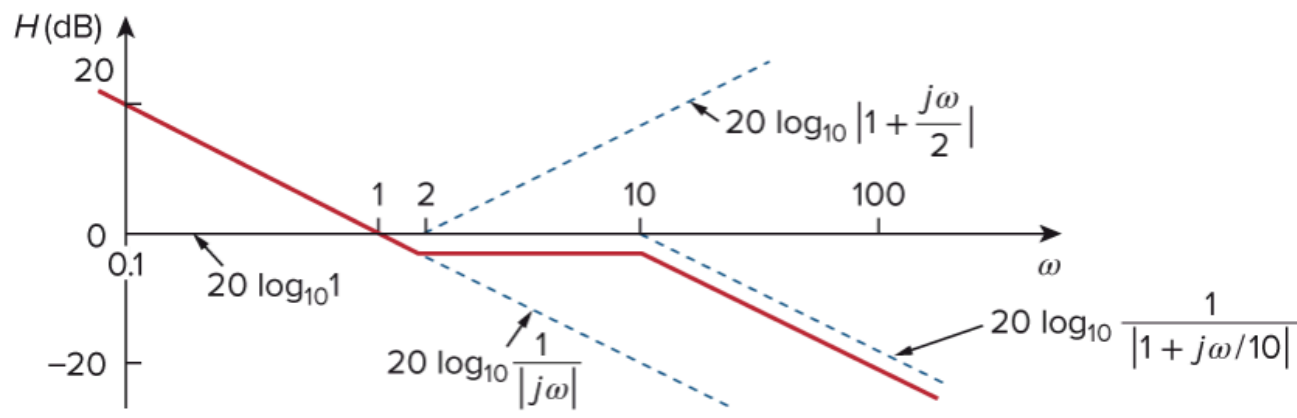
$$H(\omega) = \frac{5(j\omega + 2)}{j\omega(j\omega + 10)}$$



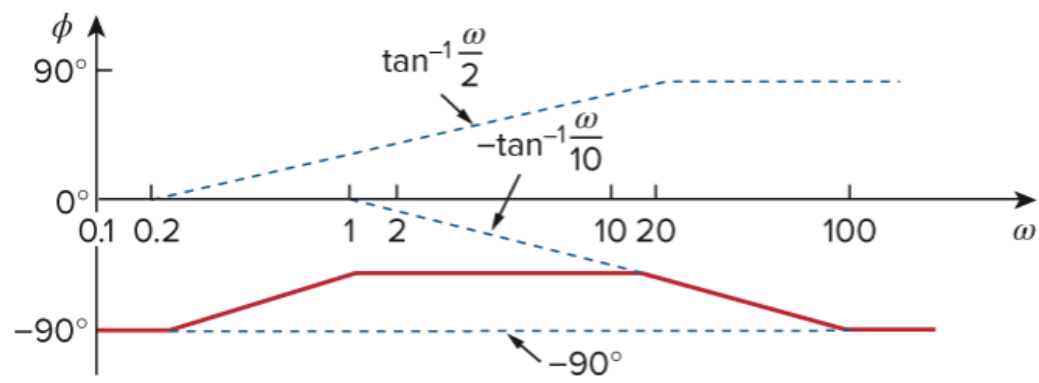
Practice Problem 14.3

Draw the Bode plots for the transfer function

$$\mathbf{H}(\omega) = \frac{5(j\omega + 2)}{j\omega(j\omega + 10)}$$

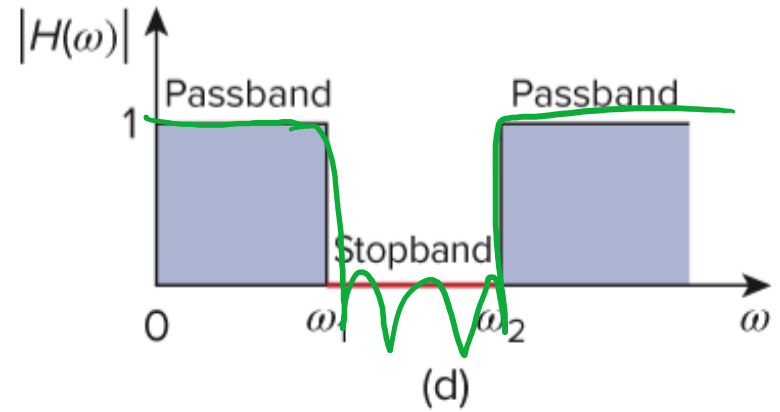
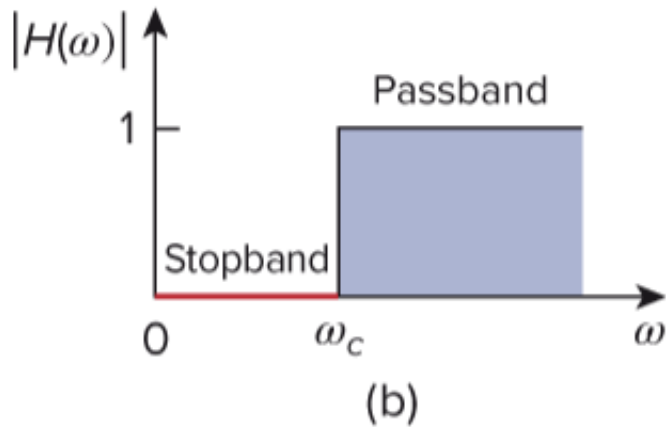
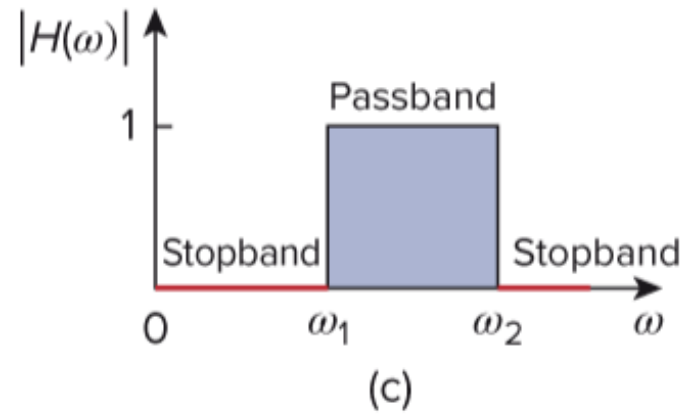
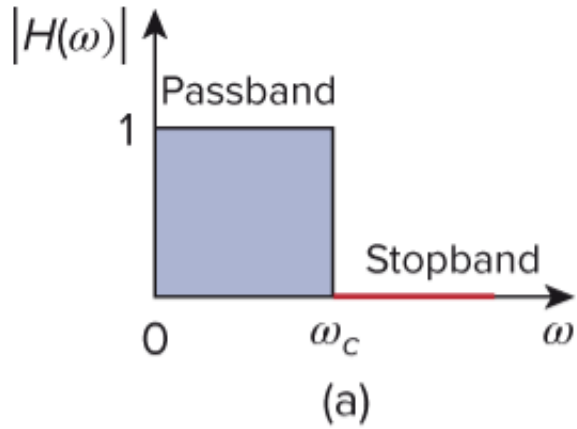
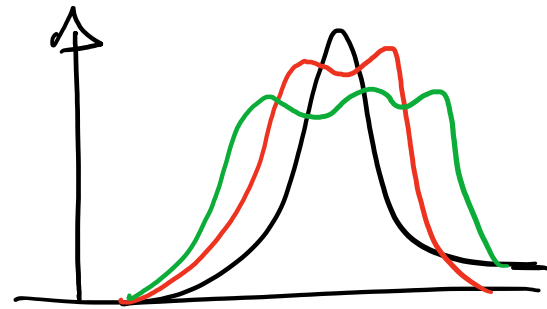


(a)



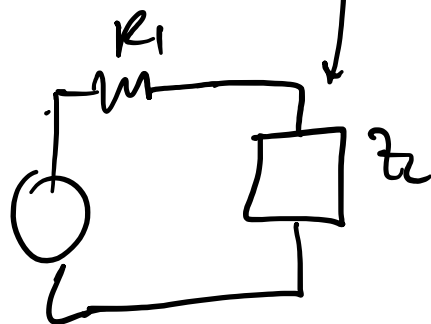
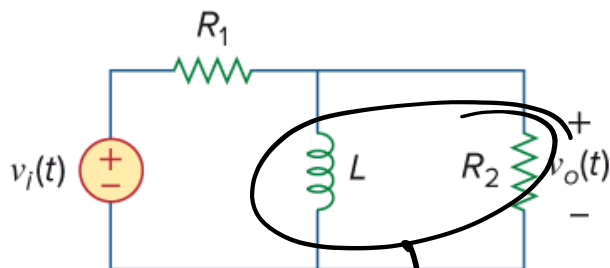
(b)

Filters



Practice Problem 14.10

For the circuit in **Fig. 14.40**, obtain the transfer function $V_o(\omega)/V_i(\omega)$. Identify the type of filter the circuit represents and determine the corner frequency. Take $R_1 = 100\ \Omega = R_2$, $L = 2\text{ mH}$.

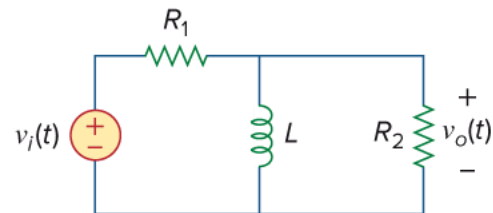


$$\begin{aligned}
 \frac{V_o}{V_i} &= \frac{\left(\frac{1}{R_2} + \frac{1}{j\omega L}\right)^{-1}}{R_1 + \left(\frac{1}{R_2} + \frac{1}{j\omega L}\right)^{-1}} = \frac{\left(\frac{j\omega L + R_2}{j\omega L R_2}\right)^{-1}}{R_1 + \left(\frac{j\omega L + R_2}{j\omega L R_2}\right)^{-1}} \\
 &= \frac{j\omega L R_2}{j\omega L + R_2} \\
 &= \frac{R_1(j\omega L + R_2)}{j\omega L + R_2} + \frac{j\omega L R_2}{j\omega L + R_2} \\
 &= \frac{j\omega L R_2}{j\omega L R_1 + R_1 R_2 + j\omega L R_2} \\
 &= \frac{j\omega L R_2}{R_1 R_2 + j\omega L (R_1 + R_2)} = \frac{j\omega L R_2 / R_1 R_2}{1 + j\omega L (R_1 + R_2) / R_1 R_2} \\
 &= \frac{j\omega L R_2 / R_1 R_2}{1 + j\omega \frac{L(R_1 + R_2)}{R_1 R_2}}
 \end{aligned}$$

$\omega_{p1} = \frac{R_1 R_2}{L(R_1 + R_2)}$

Practice Problem 14.10

For the circuit in **Fig. 14.40**, obtain the transfer function $V_o(\omega)/V_i(\omega)$. Identify the type of filter the circuit represents and determine the corner frequency. Take $R_1 = 100\ \Omega = R_2$, $L = 2\ \text{mH}$.



Answer: $\frac{R_2}{R_1 + R_2} \left(\frac{j\omega}{j\omega + \omega_c} \right)$, high-pass filter

$$\omega_c = \frac{R_1 R_2}{(R_1 + R_2)L} = 25 \text{ krad/s.}$$

Review of Course Topics

- Units
- Circuit elements (R,L,C)
- Circuit Laws (KCL, KVL, $P = VI$)
- Solving circuits (node voltage, mesh current)
- Op-amps: ideal and non-ideal
- Types of circuits to solve:
 - DC
 - Step response (over, under, critically damped): diff eq.
 - Sinusoidal steady state (phasors)
- Complex #s, impedance, power in phasor domain
- Frequency response

Final exam topics

Lecture Schedule

Section A1 – Prof. Miloš Popović, Section A2 – Prof. Mark Horenstein, Section A3 – Prof. Min-Chang Lee

Lec	Date		Topic	Reading: Chapter
	Sec. A1	Sec. A2,A3		
1	9/5	9/6	System of Units; Charge, Current and Voltage; Power and Energy; Circuit Elements; Ohm's law	Chapter 1, 2.1–2.2
2	9/8	9/11	KVL, KCL, Resistors in Series and voltage division, Resistors in parallel and current division	2.3–2.6,
3	9/12	9/13	Node-Voltage Method, Solving circuits with linear algebra	3.1–3.3
4	9/14	9/18	Mesh-current method, Application: Transistors, LED	3.4–3.7, 3.9-3.10
5	9/19	9/20	Circuit theorems: Linearity, superposition, source transformation	4.1–4.4
6	9/21	9/25	Thevenin & Norton theorems	4.5–4.7
7	9/26	9/27	Maximum Power Transfer, Examples: Source modeling, Bridge circuits, Interface circuits	4.8, 4.10–4.11
8	9/28	10/2	Introduction to operational amplifiers, Inverting and non-inverting amplifiers	5.1–5.5
9	10/3	10/4	Op-amp circuit analysis, Examples: Voltage follower, Summing and Differencing Amplifiers,	5.6–5.7
10	10/6	10/10	Cascaded OP AMP circuits	5.7-5.8
11	10/12	10/11	Op-amp circuit design, Applications: D/A conversion, Instrumentation amplifier.	5.10-5.11
12	10/17	10/16	MIDTERM EXAM 1 (Sections 1 & 2) Introduction to Capacitors, Inductors Applications: Integrator, Differentiator	Chapter 6
13	10/19	10/18	First order circuits: Source free RL and RC circuits	7.1–7.3
14	10/24	10/23	Singularity functions, RL and RC step response	7.4–7.6
15	10/26	10/25	First order op-amp circuits	7.7, 7.9–7.10
16	10/31	10/30	Intro to second order circuits Series/Parallel RLC circuits, damping	8.1–8.4

Final exam topics

Lecture Schedule

Section A1 – Prof. Miloš Popović, Section A2 – Prof. Mark Horenstein, Section A3 – Prof. Min-Chang Lee

Lec	Date		Topic	Reading: Chapter
	Sec. A1	Sec. A2,A3		
18	11/7	11/6	Sinusoidal steady state and phasors Phasor relations for circuit elements	9.1–9.4
19	11/9	11/8	Impedance and Admittance	9.5–9.8
20	11/14	11/13	MIDTERM EXAM 2 (Sections 1 & 2) Circuit analysis techniques with phasors: Thevenin and Norton.	10.1–10.6
21	11/16	11/15	OP AMP AC Circuits, maximum average power transfer	10.7, 11.3
22	11/21	11/20	Intro to filter circuits: Low-pass filters, High-pass filters, Decibel and Bode plots	14.1–14.3, 14.7
23	11/28	11/27	Band-pass filters, RLC frequency response, Resonance	14.4, 14.7
24	11/30	11/29	Active Filters	14.8
25	12/5	12/4	Filter design, Applications	14.12, Notes
26	12/7	12/6	Mutual inductance and transformers	13.1–13.5
27	12/12	12/11	Mutual inductance and transformers, Applications	notes
28	TBA	TBA	Review for final exam	
	TBA	TBA	FINAL EXAM	

Prep for final

— practice exam

- HW10 (not due); will review in review session
- Review session → doodle poll.
- Office hours between now and exam
 - Wed Dec 13 2:30-3:30pm PHO726
 - Thu Dec 14 2:30-3:30pm PHO726
 - Fri Dec 15 2:30-3:30pm PHO726
 - Mon Dec 18 1:30-3:30pm PHO726
 - Tue Dec 19 9:00-10:00am PHO726
- Exam: emphasis on last 1/3.