

EK 307: Electric Circuits

Fall 2017

Lecture 23

Dec 5, 2017

Milos Popovic

Department of Electrical and Computer Engineering

Boston University

Administrivia

- Last day of class Tue, Dec 12
- Final Exam: Tue, Dec 19, 3-5pm, PHO203

Last Lecture (22): Chapter 9

1. **Chapter 9 & 10 – Sinusoidal Steady State Circuits; Impedance/Admittance**

Today

- Chapter 10:
 - Thevenin and Norton in phasor domain
 - Active circuits (op amps)
- Chapter 11 (Sec 11.1 to 11.3):
 - Power in the phasor domain
 - Max power transfer
- Chapter 14:
 - Frequency response and intro to filter circuits

Solving AC Circuits

(Chapter 10)

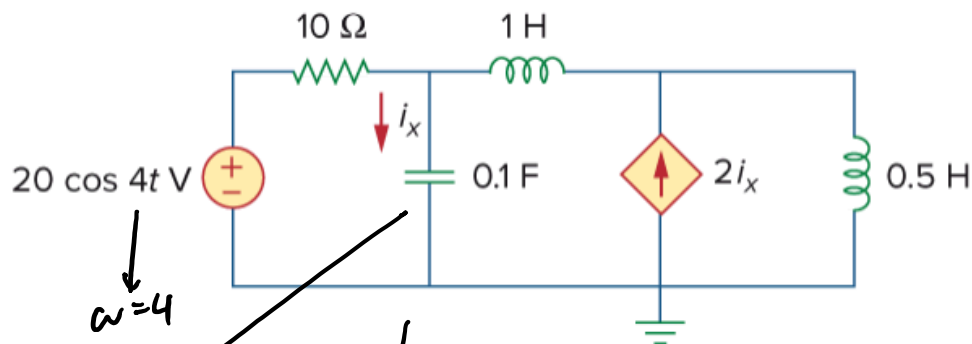
Steps to Analyze AC Circuits:

1. Transform the circuit to the phasor or frequency domain.
2. Solve the problem using circuit techniques (nodal analysis, mesh analysis, superposition, etc.).
3. Transform the resulting phasor to the time domain.

Node voltage method

Example 10.1

Find i_x in the circuit of Fig. 10.1 using nodal analysis.



$$\textcircled{1}: \frac{20\angle 0^\circ - V_1}{10} = \frac{V_1 - V_2}{j4} + \frac{V_1}{-j2.5}$$

$$\textcircled{2}: \frac{V_1 - V_2}{j4} + 2 \frac{V_1}{-j2.5} = \frac{V_2}{j2}$$

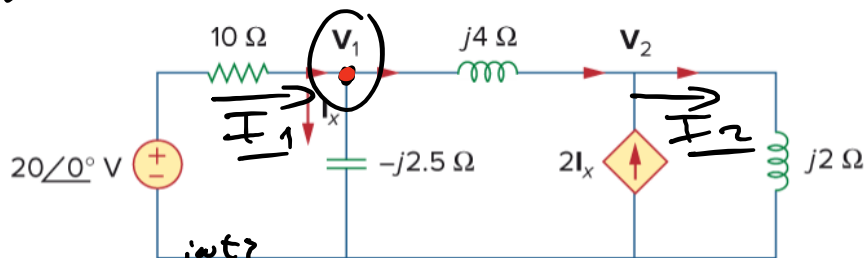
$$\underline{I}_x = \frac{V_1}{-j2.5}$$

$$\begin{aligned} \frac{20\angle 0^\circ - V_1}{10} &= \frac{V_1 - V_2}{j4} + \frac{V_1}{-j2.5} \\ \frac{V_1 - V_2}{j4} + 2 \frac{V_1}{-j2.5} &= \frac{V_2}{j2} \end{aligned}$$

$$\begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

$\omega = 4$
 $Z_C = \frac{1}{j\omega C}$
 $= -j \frac{1}{4 \cdot 0.1} = -j2.5 \Omega$

Find impedances

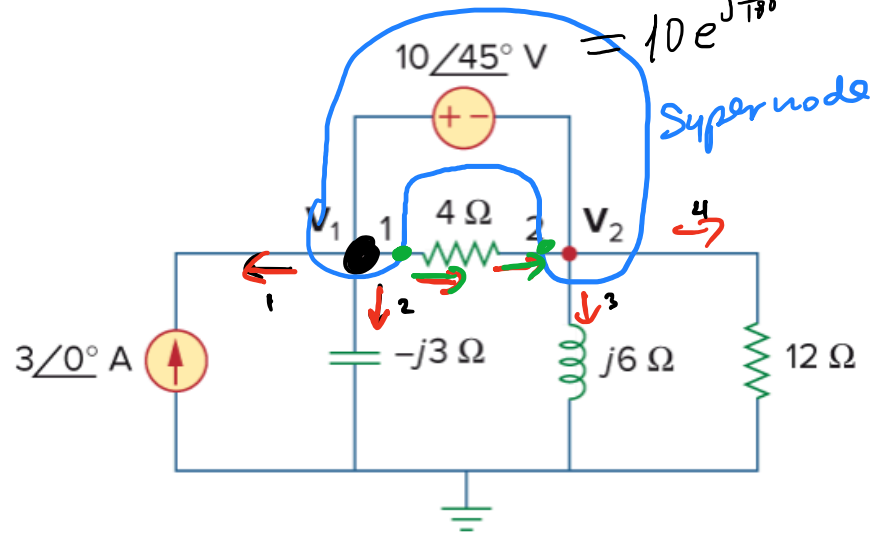


$i_x(t) = \text{Re}\{ \underline{I}_x e^{j\omega t} \}$
 $= \text{Re}\{ 10 e^{j(\omega t - 45^\circ)} \}$ say $10 \angle -45^\circ$
 $i_x(t) = 10 \cos(\omega t - 45^\circ)$

$$\underline{I}_x = \frac{V_1}{-j2.5}$$

Example 10.2

Compute V_1 and V_2 in the circuit of Fig. 10.4.



$$\underline{V_2} = \underline{V_1} - 10\angle 45^\circ$$

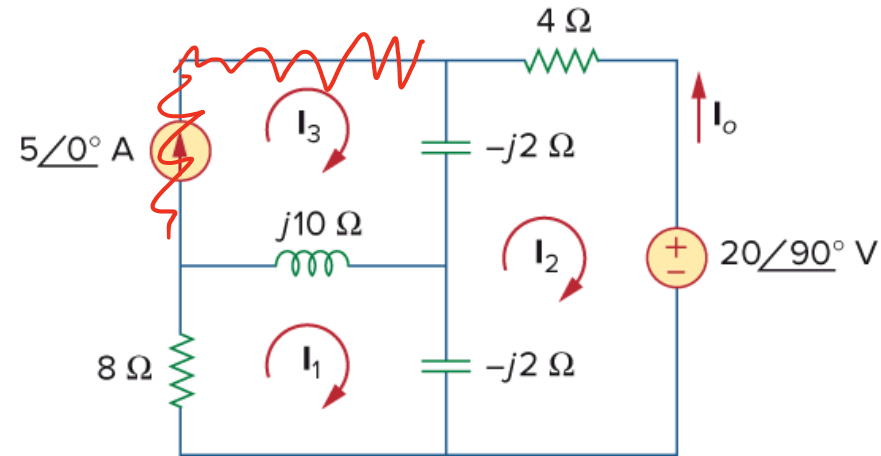
$$-3\angle 0^\circ + \frac{\underline{V_1}}{-j3} + \frac{\underline{V_1} - 10\angle 45^\circ}{j6} + \frac{\underline{V_1} - 10\angle 45^\circ}{12} = 0$$

$\downarrow$ 1 2 3 4

$$\underline{V_2} = \underline{V_1} - 10\angle 45^\circ$$

Example 10.3

Determine current $\mathbf{I}_o$ in the circuit of **Fig. 10.7** using mesh analysis.



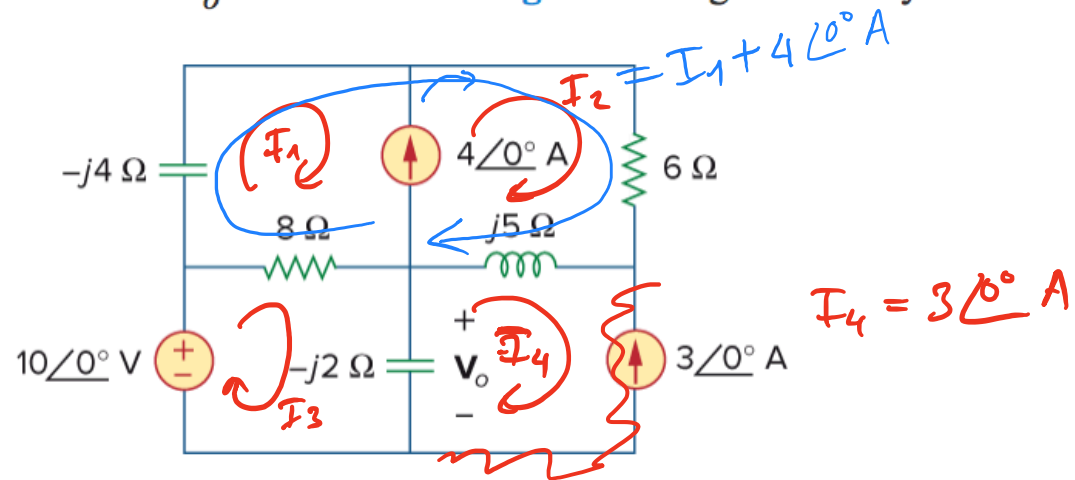
2 eqns bc $\underline{I}_3 = 5 \angle 0^\circ \text{ A}$, $i_3(t) = 5 \cos(\omega t) \text{ A}$

$\Rightarrow \begin{bmatrix} + \end{bmatrix} \begin{bmatrix} \underline{I}_2' \end{bmatrix} = \begin{bmatrix} 0 \end{bmatrix}$

$\hookrightarrow \underline{I}_o = -\underline{I}_2$

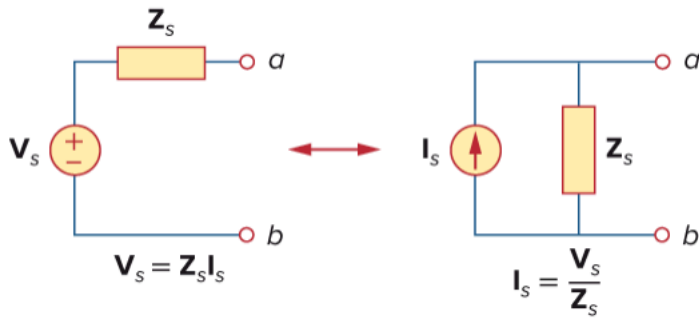
Example 10.4

Solve for V_o in the circuit of Fig. 10.9 using mesh analysis.



Source transformations

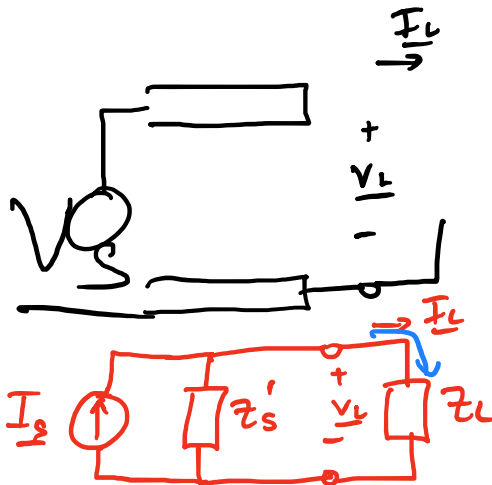
$$\underline{V}_s = \underline{Z}_s \underline{I}_s \quad \Leftrightarrow \quad \underline{I}_s = \frac{\underline{V}_s}{\underline{Z}_s}$$



Same if:

$$\underline{V}_s \equiv \underline{Z}_s \underline{I}_s$$

$$\underline{Z}_s = \underline{Z}_s'$$



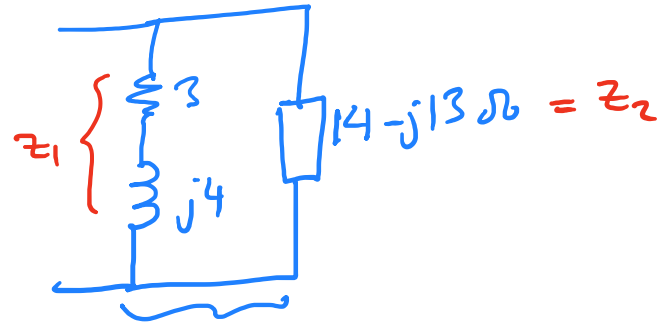
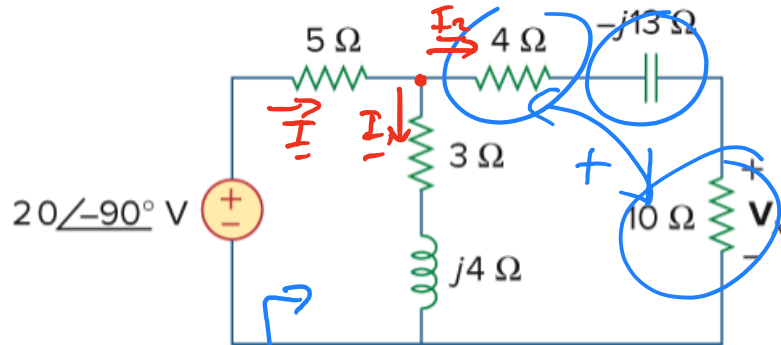
$$\underline{V}_L = \frac{Z_L}{Z_s + Z_L} \underline{V}_s$$

$$\underline{V}_L = \frac{1}{\frac{1}{Z_L} + \frac{1}{Z_s'}} \underline{I}_s = \frac{Z_L Z_s'}{Z_s' + Z_L} \underline{I}_s$$

$$\underline{I}_L = \frac{\frac{1}{Z_L}}{\frac{1}{Z_L} + \frac{1}{Z_s'}} \underline{I}_s = \frac{Y_L}{Y_L + Y_s} \underline{I}_s = \frac{Z_s'}{Z_s' + Z_L} \underline{I}_s$$

Example 10.7

Calculate V_x in the circuit of **Fig. 10.17** using the method of source transformation.



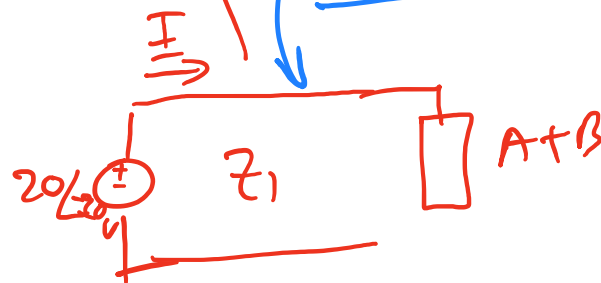
$A = 5$

$$\left(\frac{1}{3+j4} + \frac{1}{14-j13} \right)^{-1} = B$$

$$z_1 I = \frac{20 \angle -90^\circ V}{A+B}$$

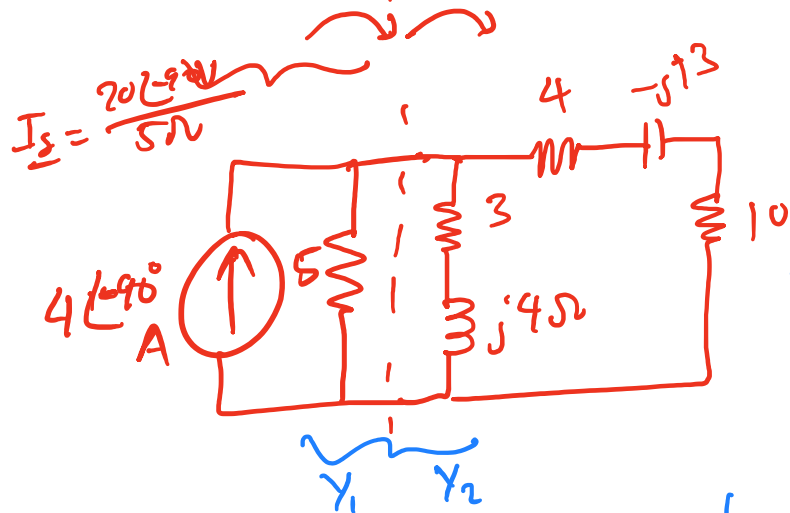
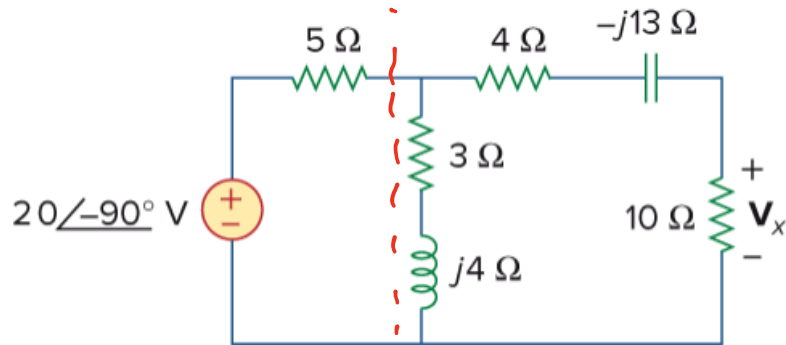
$$I_2 = \frac{z_1}{z_2 + z_1} I = \frac{Y_2}{Y_1 + Y_2} I$$

$$V_x = 10 I_2$$



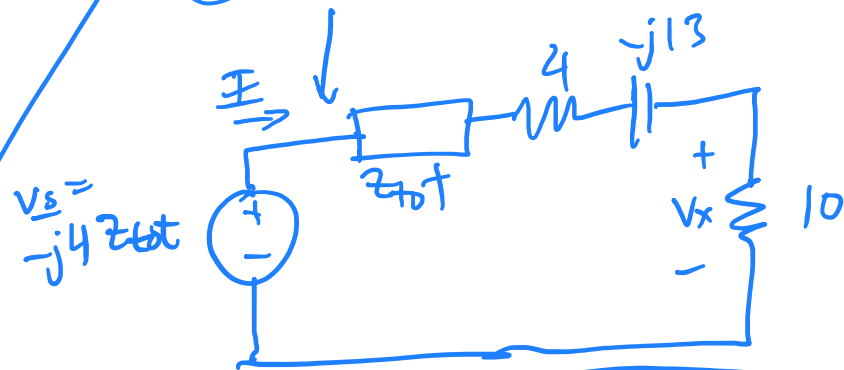
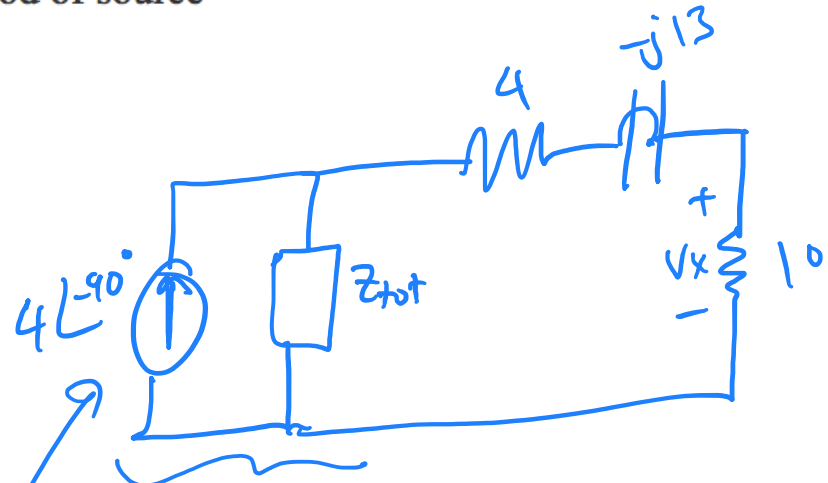
Example 10.7

Calculate V_x in the circuit of **Fig. 10.17** using the method of source transformation.



$$Y_{tot} = Y_1 + Y_2 = \frac{1}{5} + \frac{1}{3+j4}$$

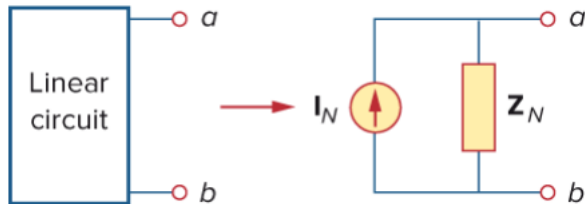
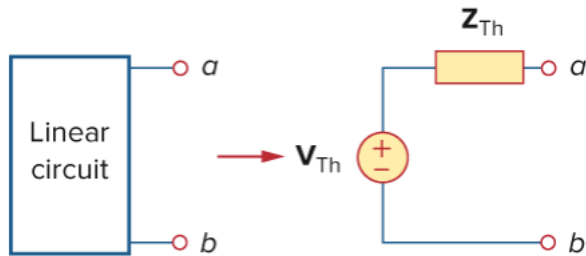
$$Z_{tot} = \frac{1}{Y_{tot}} = \left(\frac{3+j4}{15+j20} \right)^{-1}$$



$$I = \frac{1}{Z_{tot} + 4 - j13 + 10} (-j4 Z_{tot})$$

$$V_x = 10 I$$

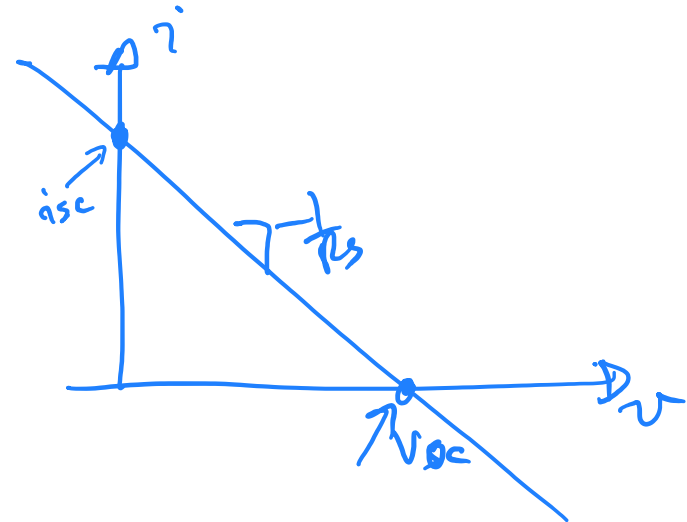
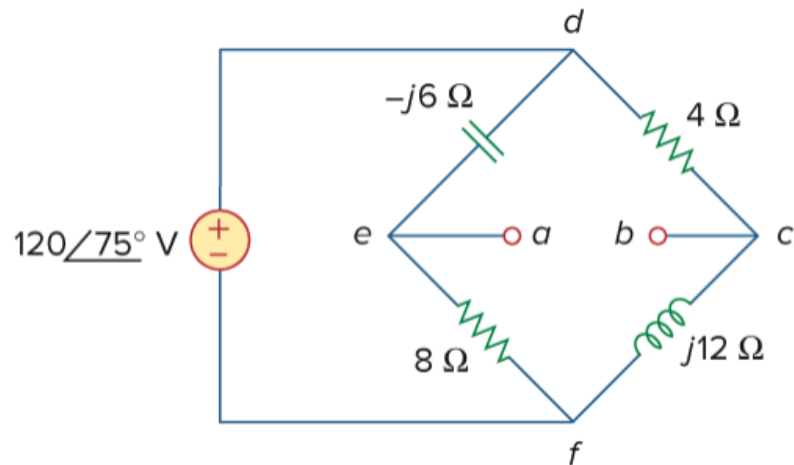
Thevenin and Norton equivalents



$$V_{Th} = Z_N I_N, \quad Z_{Th} = Z_N$$

Example 10.8

Obtain the Thevenin equivalent at terminals $a-b$ of the circuit in Fig. 10.22.



Example 10.8

Obtain the Thevenin equivalent at terminals $a-b$ of the circuit in Fig. 10.22.

$\underline{V}_S = 120 \angle 75^\circ \text{ V}$

$Z_2 = -j6 \Omega$, $Z_1 = 8 \Omega$, $4 \Omega = Z_4$, $j12 \Omega = Z_3$

$\underline{V}_e = \frac{8}{8 - j6} 120 \angle 75^\circ \text{ V} = \frac{Z_1}{Z_1 + Z_2} \underline{V}_S$

$\underline{V}_c = \frac{Z_3}{Z_3 + Z_4} \underline{V}_S = \frac{j12}{j12 + 4} 120 \angle 75^\circ \text{ V}$

$\underline{V}_{oc} = \underline{V}_e - \underline{V}_c$

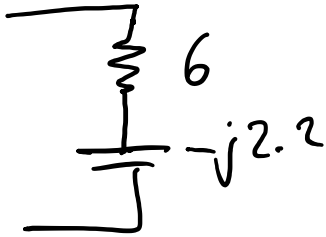
$\underline{Z}_5 = \left(\frac{1}{8} + \frac{1}{-j6} \right)^{-1}$, $\underline{Z}_6 = \left(\frac{1}{4} + \frac{1}{j12} \right)^{-1}$

$\underline{Z}_{eq} = \underline{Z}_5 + \underline{Z}_6 = \left(\frac{1}{8} + \frac{1}{-j6} \right)^{-1} + \left(\frac{1}{4} + \frac{1}{j12} \right)^{-1}$

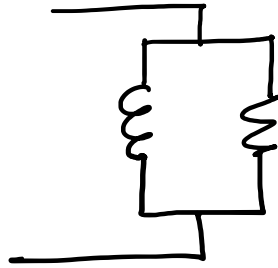
$= 5 \angle -60^\circ + 4 \angle -30^\circ = 5 \left(\frac{1}{2} - j\frac{\sqrt{3}}{2} \right) + 4 \left(\frac{\sqrt{3}}{2} - j\frac{1}{2} \right)$

$= \underline{6 - j2.2}$

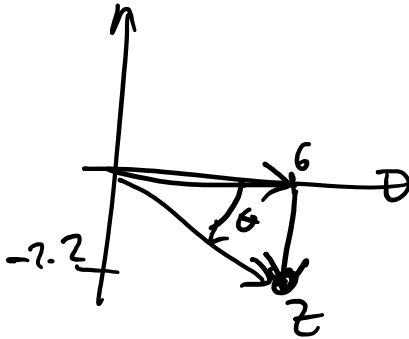
$e^{-j60^\circ} = \cos 60^\circ - j \sin 60^\circ$



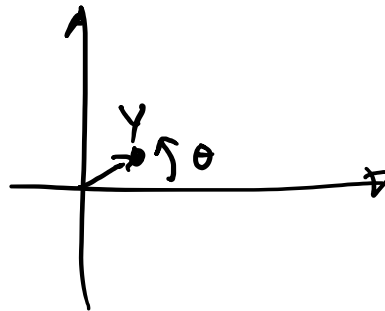
$$Z = 6 - j2.2$$

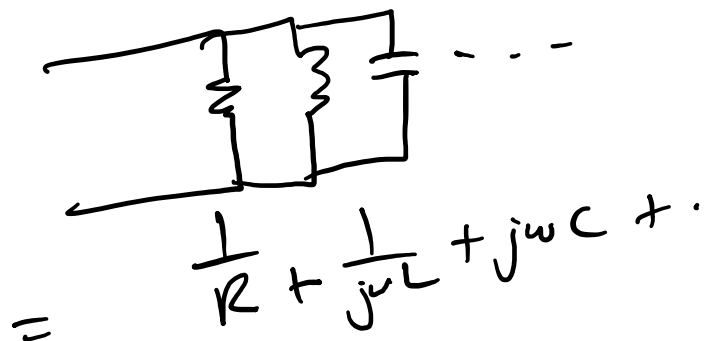
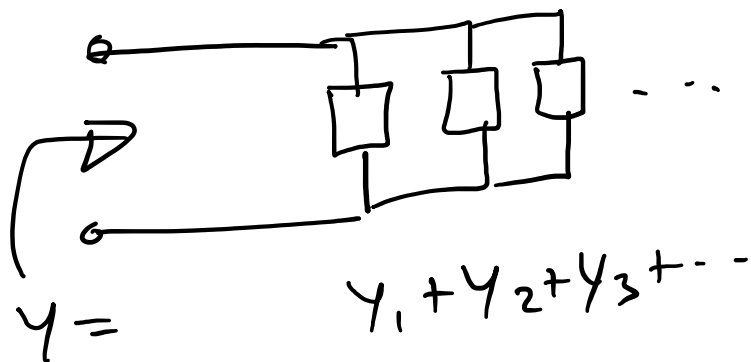


$$Y = \frac{1}{6 - j2.2} = \underset{>0}{G} + j \underset{>0}{B}$$



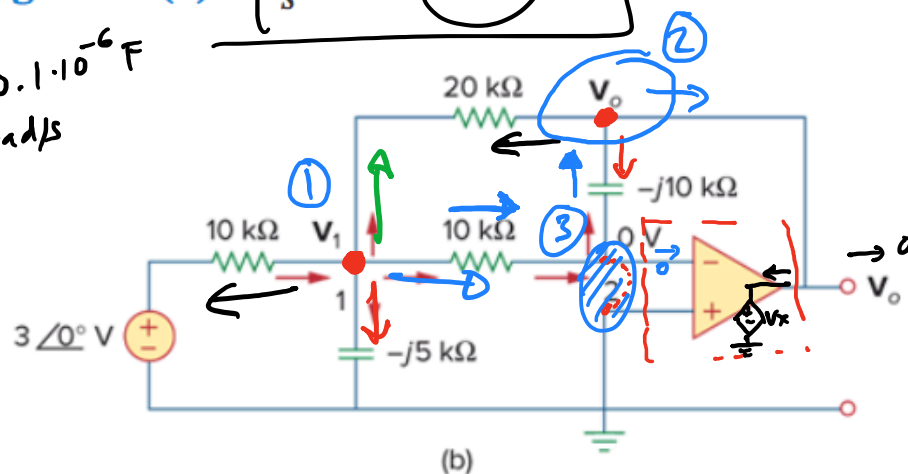
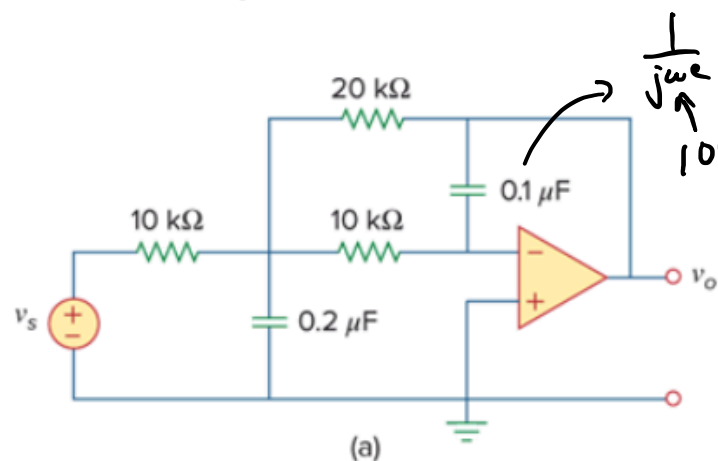
$\xrightarrow{1/Z}$





Example 10.11

Determine $v_o(t)$ for the op amp circuit in Fig. 10.31(a) if $v_s = 3 \cos 1000t$ V.



$$\underline{V_s} = 3 \angle 0^\circ$$

$$\textcircled{1}: \frac{V_1 - 3 \angle 0^\circ}{10k} + \frac{V_1}{-j5k} + \frac{V_1 - 0}{10k} + \frac{V_1 - V_o}{20k} = 0$$

~~$$\textcircled{2}: \frac{V_o - V_1}{20k} + \frac{V_o - 0}{-j10k} +$$~~

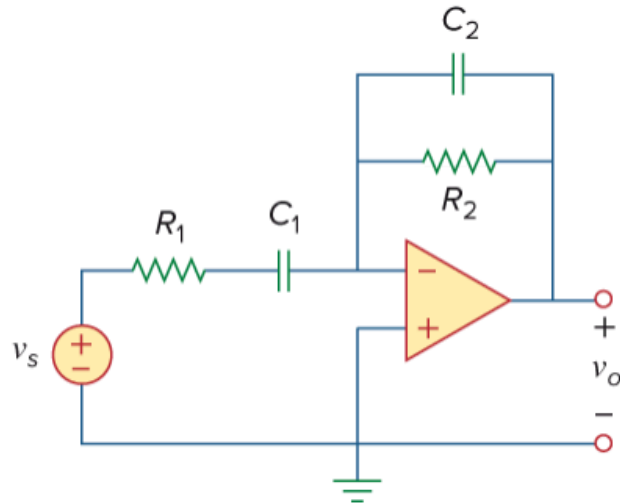
$$\textcircled{3}: \frac{V_1 - 0}{10k\Omega} = \frac{0 - V_o}{-j10k}$$

$$V_1 = \frac{-10k}{-j10k} V_o = -j V_o$$

Example 10.12

Compute the closed-loop gain and phase shift for the circuit in **Fig. 10.33**.

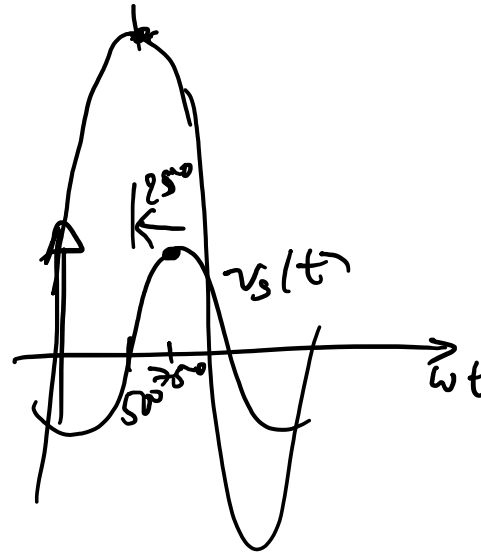
Assume that $R_1 = R_2 = 10 \text{ k}\Omega$, $C_1 = 2 \mu\text{F}$, $C_2 = 1 \mu\text{F}$, and $\omega = 200 \text{ rad/s}$.



$$\frac{v_o}{v_s} = \frac{1000 \cos(\omega t - 50^\circ)}{3 \cos(\omega t - 75^\circ)}$$

$$\frac{V_o}{V_s} = \frac{1000 e^{-j50^\circ}}{3 e^{-j75^\circ}} = e^{-j50^\circ}$$

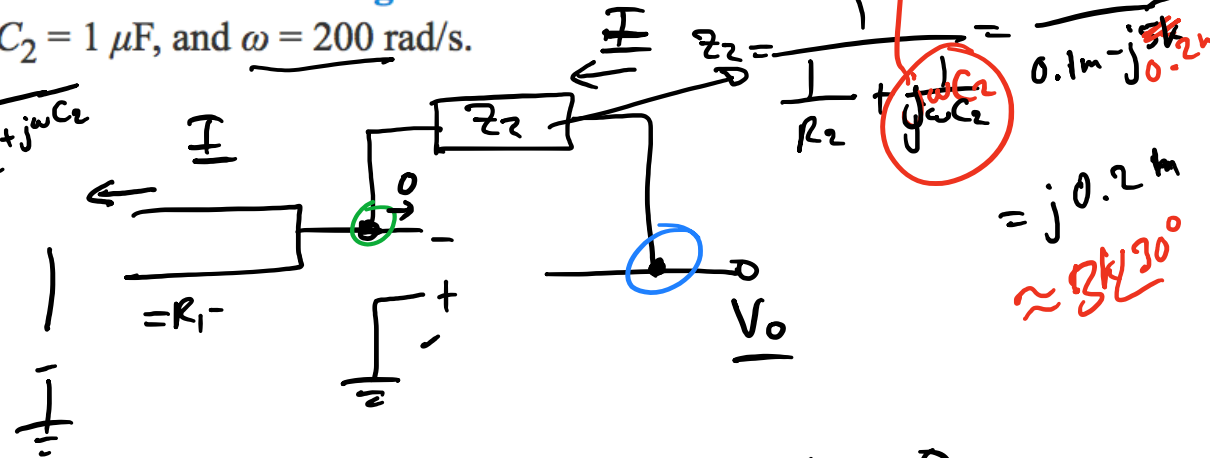
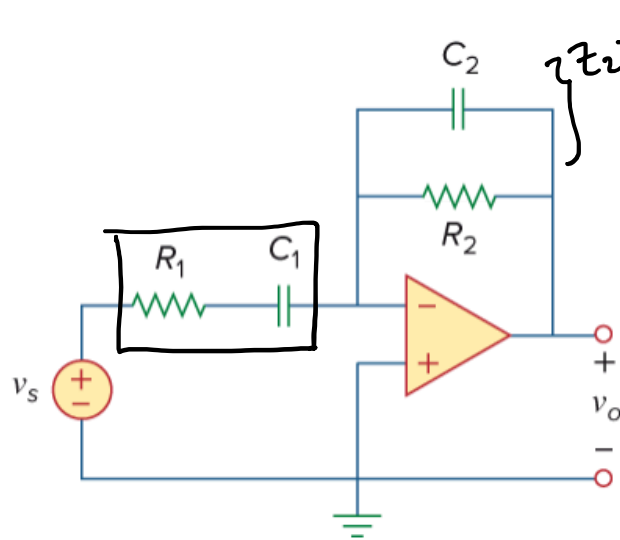
$$\underline{G} = \frac{V_o}{V_s} = 333 e^{+j25^\circ}$$



Example 10.12

Compute the closed-loop gain and phase shift for the circuit in Fig. 10.33.

Assume that $R_1 = R_2 = 10 \text{ k}\Omega$, $C_1 = 2 \mu\text{F}$, $C_2 = 1 \mu\text{F}$, and $\omega = 200 \text{ rad/s}$.



$$\frac{V_o}{V_s} = -\frac{Z_2}{Z_1} \quad \begin{cases} I = \frac{V_o - 0}{Z_2} \\ I = \frac{0 - V_s}{Z_1} \end{cases}$$

$$\frac{V_o}{V_s} = \frac{j0.2\text{m} \angle 90^\circ}{10\text{k} \angle -25^\circ} = \frac{0.2\text{m} \angle 115^\circ}{10\text{k}} = 0.02 \times 10^{-3} \angle 115^\circ = 2 \times 10^{-5} \angle 115^\circ$$

$$v_s = 1 \cos(200t)$$

$$v_o = 10^{-8} \cos(200t + 115^\circ)$$

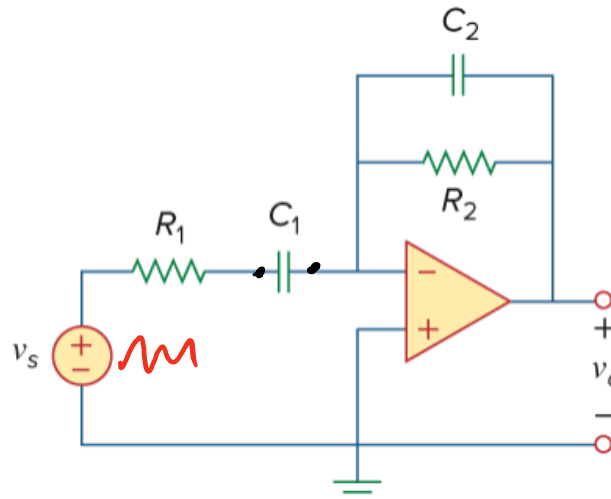
For 200 rad/s
 $\approx 30 \text{ Hz}$
 $\rightarrow$

$$\frac{V_o}{V_s} = \frac{0.02 \times 10^{-3}}{10^3} \angle 115^\circ = 2 \times 10^{-8} \angle 115^\circ$$

Example 10.12

Compute the closed-loop gain and phase shift for the circuit in **Fig. 10.33**.

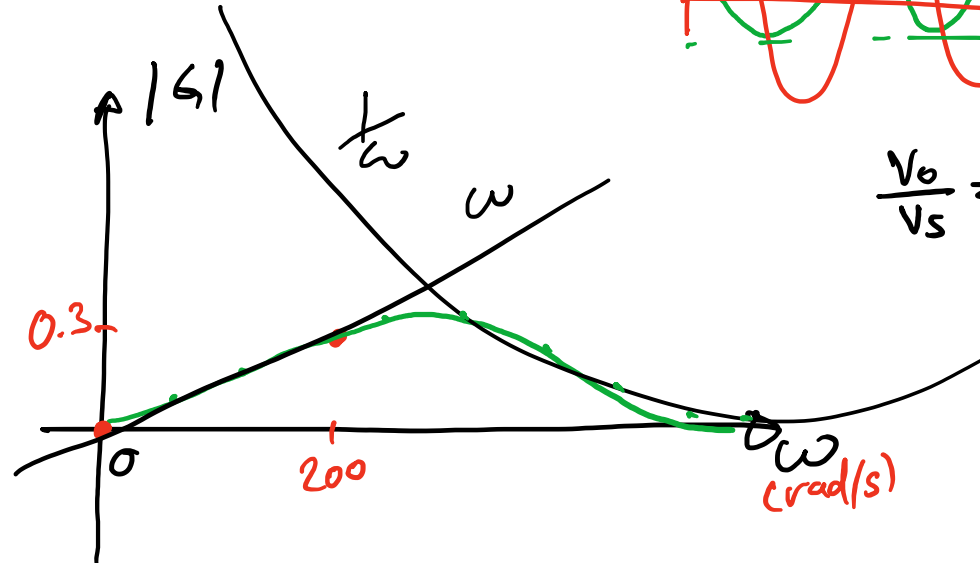
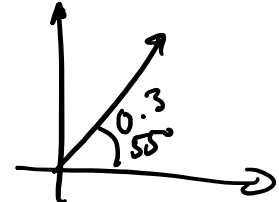
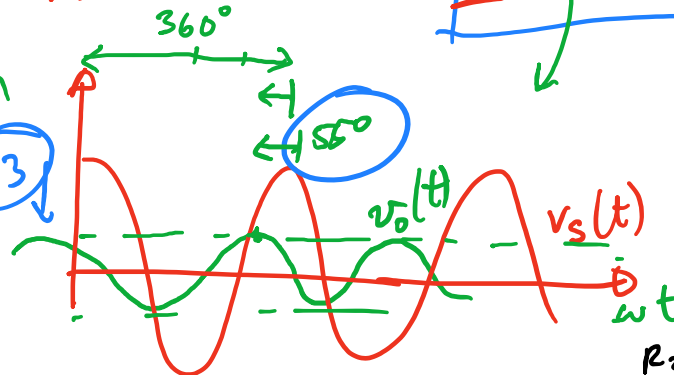
Assume that $R_1 = R_2 = 10 \text{ k}\Omega$, $C_1 = 2 \mu\text{F}$, $C_2 = 1 \mu\text{F}$, and $\omega = 200 \text{ rad/s}$.



At $\omega = 0$: $\underline{G} = 0$

At $\omega = 200 \text{ rad/s}$: $\underline{G} = 0.3 \angle 55^\circ$

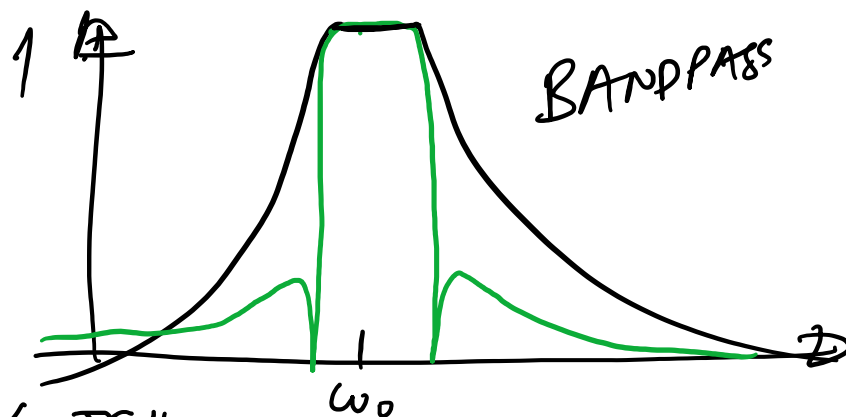
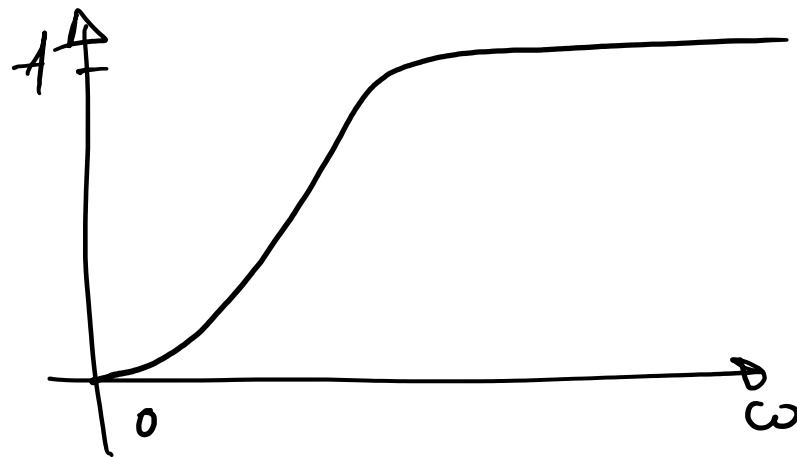
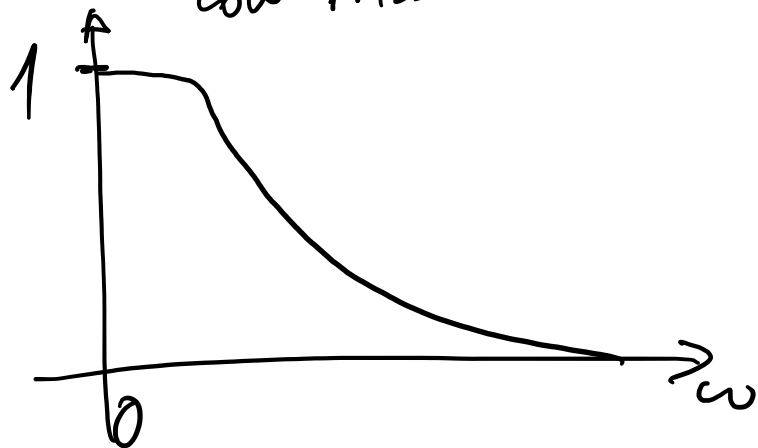
$|\underline{G}| = 0.3$



$$\frac{V_o}{V_s} = \frac{-Z_2}{Z_1} = \frac{\frac{R_2 \frac{1}{j\omega C_2}}{R_2 + \frac{1}{j\omega C_2}}}{R_1 + \frac{1}{j\omega C_1}} = \frac{R_2 \frac{1}{j\omega C_2} \left(\frac{j\omega C_2}{R_2 + j\omega C_2} \right)}{R_1 + \frac{1}{j\omega C_1}}$$

FILTERS

LOW PASS



BANDPASS

BANDSTOP / NOTCH



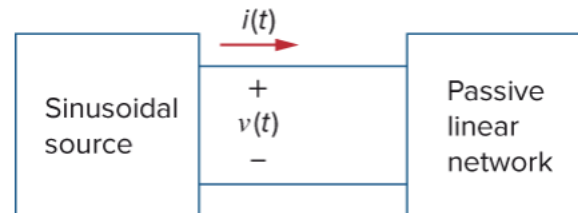
Chapter 11: Power in phasor domain

Instantaneous and average power

$$p(t) = v(t)i(t)$$

$$v(t) = V_m \cos(\omega t + \theta_v)$$

$$i(t) = I_m \cos(\omega t + \theta_i)$$



Instantaneous and average power

$$v(t) = V_m \cos(\omega t + \theta_v)$$

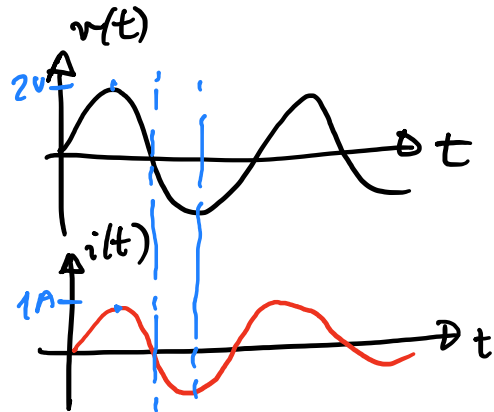
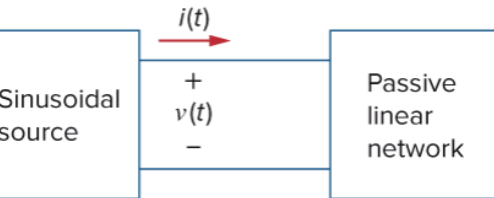
$$i(t) = I_m \cos(\omega t + \theta_i)$$

$$p(t) = \underline{v(t)} \underline{i(t)} = V_m I_m \underline{\cos(\omega t + \theta_v)} \underline{\cos(\omega t + \theta_i)}$$

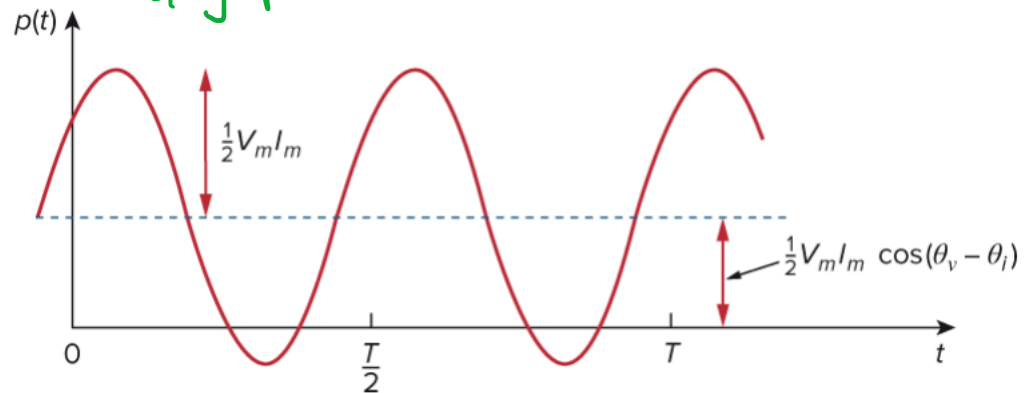
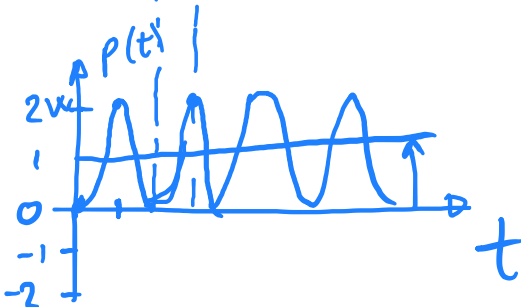
$$\cos A \cos B = \frac{1}{2} [\cos(A - B) + \cos(A + B)]$$

Instantaneous power:

$$p(t) = \underbrace{\frac{1}{2} V_m I_m \cos(\theta_v - \theta_i)}_{\text{avg power}} + \frac{1}{2} V_m I_m \cos(2\omega t + \theta_v + \theta_i)$$



i
 v R
 $p(t)$ burned in resistor W (J/s)

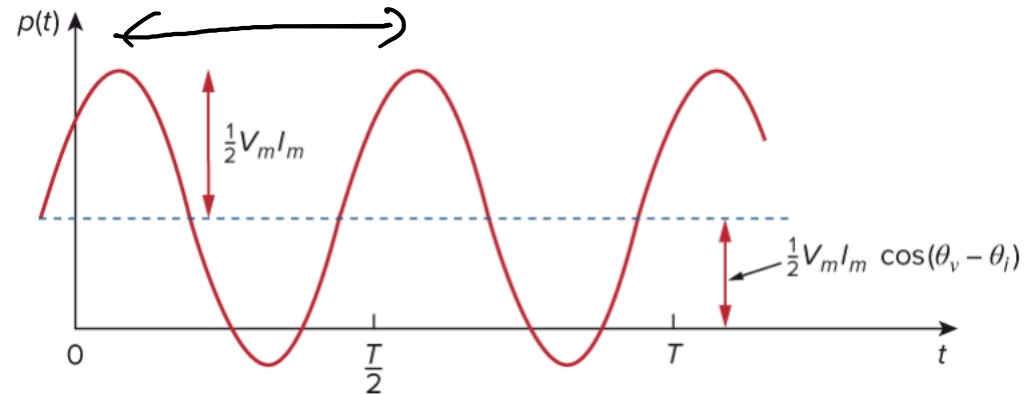
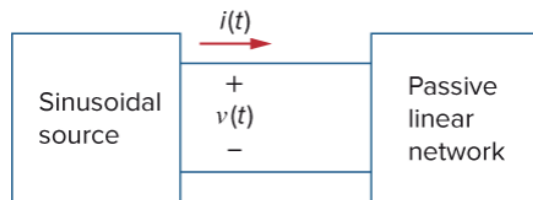


Instantaneous and average power

$$v(t) = V_m \cos(\omega t + \theta_v)$$

$$i(t) = I_m \cos(\omega t + \theta_i)$$

$$p(t) = \frac{1}{2} V_m I_m \cos(\theta_v - \theta_i) + \frac{1}{2} V_m I_m \cos(2\omega t + \theta_v + \theta_i)$$



$$P = \frac{1}{T} \int_0^T p(t) dt$$

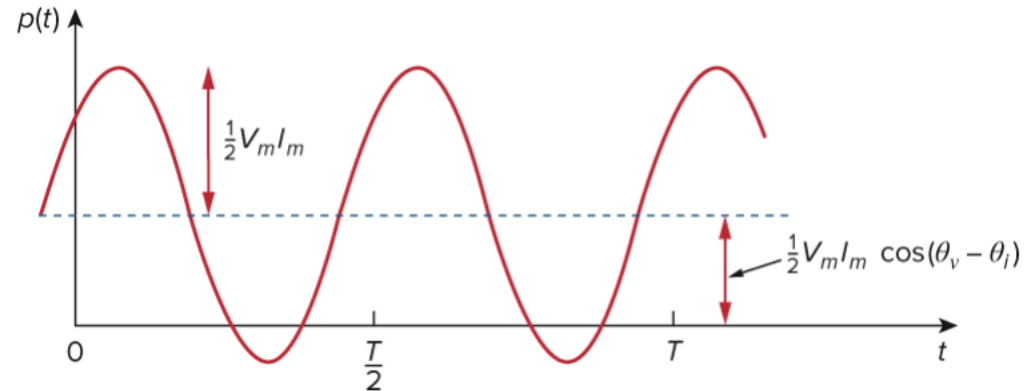
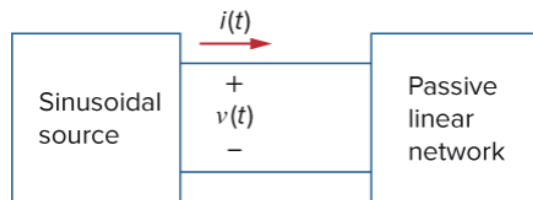
$$P = \frac{1}{2} V_m I_m \cos(\theta_v - \theta_i)$$

Instantaneous and average power

$$v(t) = V_m \cos(\omega t + \theta_v)$$

$$i(t) = I_m \cos(\omega t + \theta_i)$$

$$p(t) = \frac{1}{2} V_m I_m \cos(\theta_v - \theta_i) + \frac{1}{2} V_m I_m \cos(2\omega t + \theta_v + \theta_i)$$



$$P = \frac{1}{2} V_m I_m \cos(\theta_v - \theta_i)$$



$$\frac{1}{2} \mathbf{V} \mathbf{I}^* = \frac{1}{2} V_m I_m \angle \theta_v - \theta_i$$

$$= \frac{1}{2} V_m I_m [\cos(\theta_v - \theta_i) + j \sin(\theta_v - \theta_i)]$$

$$P = \frac{1}{2} \text{Re}[\mathbf{V} \mathbf{I}^*] = \frac{1}{2} V_m I_m \cos(\theta_v - \theta_i)$$