

APPLIED PHYSICS

Meta-optics achieves RGB-achromatic focusing for virtual reality

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Virtual and augmented realities are rapidly developing technologies, but their large-scale penetration will require lightweight optical components with small aberrations. We demonstrate millimeter-scale diameter, high-NA, submicron-thin, metasurface-based lenses that achieve diffraction-limited achromatic focusing of the primary colors by exploiting constructive interference of light from multiple zones and dispersion engineering. To illustrate the potential of this approach, we demonstrate a virtual reality system based on a home-built fiber scanning near-eye display.

INTRODUCTION

Optical lenses are in demand more than ever before. They are being widely used in electronic devices such as smart phones. Unlike electronics that has rapidly evolved and shrunk in size following the Moore's law over the past decades, the appearance and the underlying physics of today's optical lenses are similar to the Nimrud lens dating back to ~3000 years ago (1, 2). Light focusing by a refractive lens relies on accumulation of propagation phase, and thus, lens thickness scales up as diameter (3). Moreover, multilens sets, such as doublets and triplets, are required to correct chromatic aberrations. Fresnel lenses have a reshaped compact form yet suffer from poor imaging quality due to their strong chromatic aberrations (2) and other limitations. Achromatic lenses, such as camera objectives, have a large form factor due to their composite nature, which imposes a bottleneck to next-generation optical systems such as wearable display in terms of footprint, imaging quality, complexity, and cost.

Metasurfaces have emerged as a platform for novel flat optics in recent years (4, 5). They are arrays of nanostructures assembled on a subwavelength scale, which can mold electromagnetic wavefronts at will. Metalenses, in particular, have been widely studied to address the challenges of conventional optics and show considerable potential for practical applications (6–8). Fundamentally different from traditional lenses, metalenses are optically thin and light and can be designed to correct monochromatic and chromatic aberrations without requiring the complexity of refractive optics by controlling the phase, amplitude, and polarization state of the transmitted light with subwavelength resolution; high numerical aperture (NA) is easy to achieve in metalenses (9). In recent works, researchers have demonstrated metalenses working in the visible based on new material platforms (10, 11) and by complementary metal-oxide semiconductor (CMOS)-compatible fabrication techniques (12) that are feasible for mass production of large-diameter metalenses.

Researchers have realized achromatic metalenses over broad bandwidth by locally engineering waveguide modes (or resonate modes)

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of meta-atoms to compensate chromatic dispersion (13–18). However, such achromatic metalenses have a diameter size of tens of micron due to limited group delay achievable with meta-atoms (19), limiting their practical use. Here, we present a general design principle to achieve large-area, multiwavelength achromatic metalenses. We demonstrate in the experiment the 2-mm-diameter red-green-blue (RGB)-achromatic transmissive metalenses. Furthermore, we demonstrate a compact virtual reality (VR) platform based on the RGB-achromatic metalens and a fiber scanning near-eye display.

RESULTS

Design principles

Traditional optical lenses suffer from chromatic aberrations limiting their imaging performance. The chromatic aberration of a refractive lens originates from the intrinsic material dispersion that causes longer wavelengths to focus at longer focal distance. In comparison, the focusing of a diffractive lens, Fresnel lens for example, is more than 10 times dispersive. Such severe chromaticity is mainly due to phase discontinuities at zone boundaries. It results in longer focal distances for shorter wavelengths (2). The form factor and the chromatic aberration of a traditional optical lens are hard to reduce at the same time. To address such a challenge, we introduce a multizone dispersion-engineered metalens (Fig. 1A) by using a design principle as described in Eq. 1

$$\tilde{E}(\omega) = \sum_{i=1}^N \left(\int_{r_{i-1}}^{r_i} t(\omega, r) e^{i\varnothing_i(\omega, r)} r dr \right) e^{i\Delta\varnothing_i(\omega)} = \sum_{i=1}^N \tilde{E}_i(\omega) e^{i\Delta\varnothing_i(\omega)} \quad (1)$$

where N is the number of zones, and r_i is the radial coordinate of each zone boundary ($r_0 = 0$); $t(\omega, r)$ characterizes the amplitude of the scattered electric field by meta-atoms at a frequency of ω ; $\varnothing_i(\omega, r)$ is the designed phase profile within the i th zone; and $\Delta\varnothing_i(\omega)$ is the phase discontinuity at the boundary between $(i - 1)$ th and i th zone [$\Delta\varnothing_1(\omega) = 0$]. The electric field $\tilde{E}(\omega)$ at the focal spot is determined by the interference of electric field within each zone [$t(\omega, r)e^{i\varnothing_i(\omega, r)}$] and the interference of the electric fields [$\tilde{E}_i(\omega)$] from N different zones (Fig. 1A). To maximize the focusing intensity $|\tilde{E}(\omega_0)|^2$ at a single frequency ω_0 , the desired phase profile within each zone should be hyperbolic, i.e., $\varnothing_i(\omega_0, r) = \omega_0 c (F(\omega_0) - \sqrt{F(\omega_0)^2 + r^2})$, where $F(\omega_0)$ is the focal length at frequency ω_0 ; in addition, the phase discontinuities at the zone boundaries should be zero, $\Delta\varnothing_i(\omega_0) = 0$.

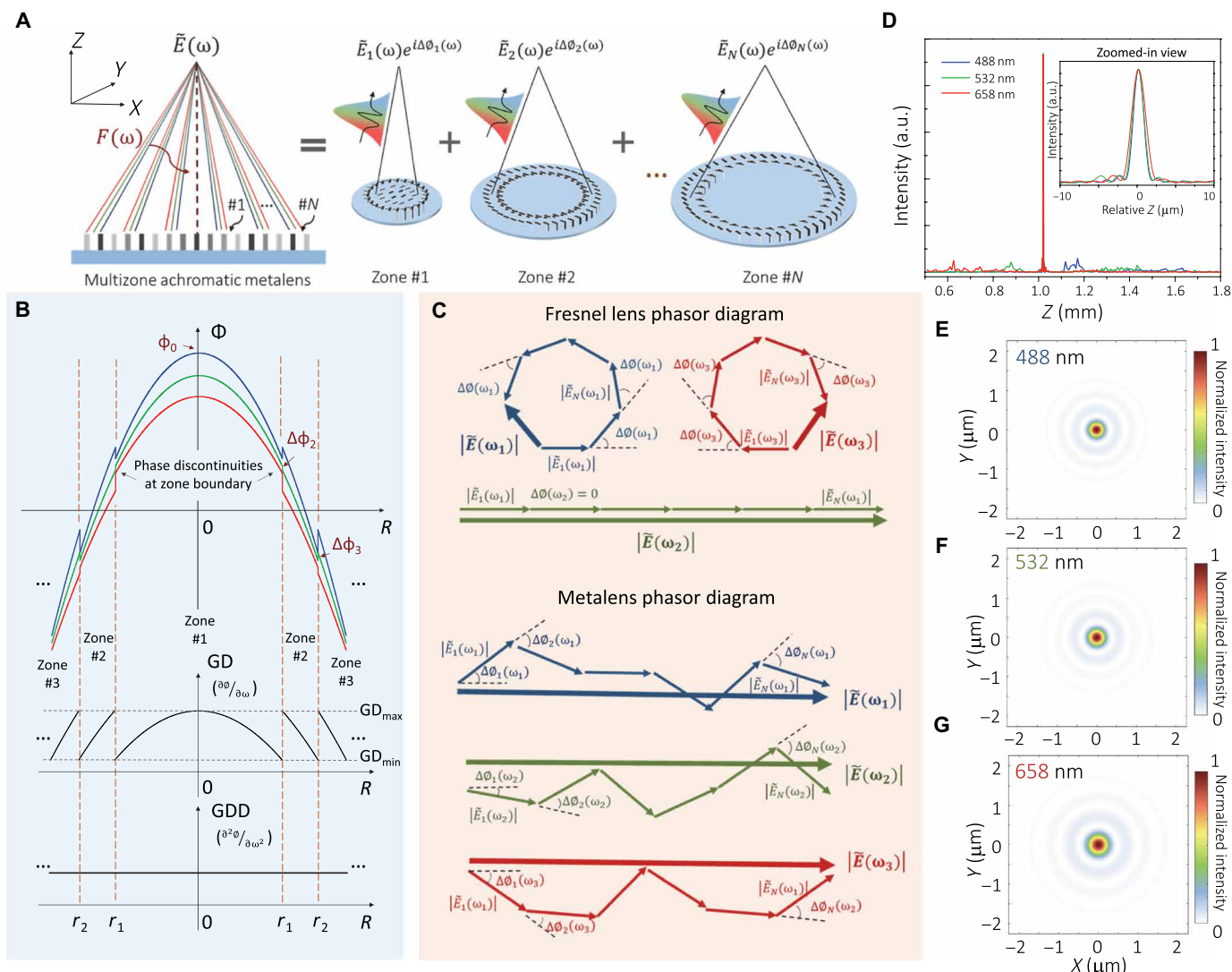


Fig. 1. Design and simulations of an RGB-achromatic metalens. (A) Schematic drawing of a multizone RGB-achromatic metalens showing achromatic focusing of RGB light coming from different lens locations. $\vec{E}(\omega)$ represents the interfered complex electric field at the focal spot of frequency ω . (B) One example of the phase profile, the group delay (GD) profile, and the group delay dispersion (GDD) profile designed for a multizone, RGB-achromatic metalens. The zone is defined by an area with continuously changed dispersion. Phase discontinuities at zone boundaries, zone transition locations, and initial phase at the lens centers require independent control. (C) Schematic drawing of a Fresnel lens phasor diagram and a metalens phasor diagram at a design focal spot. Phase discontinuities of a metalens can be independently engineered without changing the dispersion within each zone. (D) Simulated focusing intensity distribution of the metalens with NA = 0.7 along its optical axis at design wavelengths of 488, 532, and 658 nm. The inset is the zoomed-in view of focusing peaks. a.u., arbitrary units. (E to G) Simulation results of the intensity profiles in the focal planes at the design wavelengths.

To achieve controlled focusing at different frequencies, we set an multiobjective optimization function as $\max(\min(|\vec{E}(\omega_i)|^2))$, where $\omega_i \in \{\omega_1, \omega_2, \dots, \omega_n\}$ is the design frequency. It means to maximize the minimum value of the focusing intensity at design frequencies. In our design, we engineered the lens phase profiles (Fig. 1B) within each zone according to Eq. 2

$$\begin{aligned} \phi_i(\omega, r) &= \frac{\omega}{c} \left(F(\omega) - \sqrt{F(\omega)^2 + r^2} \right) + \phi_0(\omega) \\ &= \frac{\omega_0}{c} \left(F(\omega_0) - \sqrt{F(\omega_0)^2 + r^2} \right) + \frac{\partial \phi_i(\omega, r)}{\partial \omega} (\omega - \omega_0) + \\ &\quad \frac{\partial^2 \phi_i(\omega, r)}{2 \partial \omega^2} (\omega - \omega_0)^2 + \phi_0(\omega) \end{aligned} \quad (2)$$

where $F(\omega)$ is the focal length at frequency ω , r is the radial coordinate, ω_0 is the center design wavelength, and $\phi_0(\omega)$ is the phase at the metalens center. This designed phase profile was realized by using spatially varied meta-atoms that can independently control phase and dispersion (group delay $\partial\phi/\partial\omega$, group delay dispersion $\partial^2\phi/\partial\omega^2$). In this way, light from an individual zone constructively interfere at a focal spot for all design frequencies. Furthermore, we engineer zone interference using an inverse design method. To be more specific, we optimize the zone transition locations r_i and the phase discontinuities $\Delta\phi_i(\omega)$ using the method of moving asymptotes, which is a gradient-based local optimization method (20). The engineered meta-atoms also allow imposing an additional $\Delta\phi_i(\omega)$ onto each zone's phase profile $\phi_i(\omega, r)$ without altering local phase gradient

and, thus, light interference within each zone, as can be seen that $\Delta\varnothing_i(\omega)$ is independent on lens location r within each zone, i.e., $\partial\Delta\varnothing_i(\omega)/\partial r = 0$. The phase discontinuity at a certain frequency ω is related to the center frequency ω_0 in a following way

$$\Delta\varnothing(\omega, r_i) = \Delta\varnothing(\omega_0, r_i) + \frac{\omega_0}{c}(F(\omega_0) - \sqrt{F(\omega_0)^2 + r_i^2}) - \frac{\omega}{c}(F(\omega) - \sqrt{F(\omega)^2 + r_i^2}) \quad (3)$$

The details of design principles are explained in the Supplementary Materials (section S1). The ability to independently engineer phase profile, dispersion within each zone, and phase discontinuities at zone boundaries rewrites the physics governing a Fresnel lens, in which these parameters cannot be independently controlled. Figure 1C shows phasor diagrams of a typical Fresnel lens and our dispersion-engineered metalens at the design focal spot highlighting their differences. The result of zone interference can be understood as lining up phasor units $[\vec{E}_i(\omega)]$ contributed by each zone with certain angles that are determined by phase discontinuities at zone boundaries $[\Delta\varnothing_i(\omega)]$. In the Fresnel lens, phase discontinuities at design frequency (ω_0) are kept zero for constructive interference. However, destructive interference occurs at other frequencies (e.g., ω_1 and ω_3) caused by their fixed nonzero phase discontinuities and intrinsic material dispersion. In comparison, in our metalens, phasor units $[\vec{E}_i(\omega)]$ within each zone and phase discontinuities $[\Delta\varnothing_i(\omega)]$ at each zone boundary are both engineered to realize the overall constructive interference at the design wavelengths.

Simulation results of large RGB-achromatic metalenses

By applying the above principles, we designed two 2-mm-diameter metalenses with NAs of 0.7 and 0.3, with the goal of focusing three primary RGB colors at the same focal length $[F(\omega) = F_0]$ while suppressing spurious focal spots elsewhere along the optical axes. Using the first three zones of an RGB-achromatic metalens for illustration, Fig. 1B shows examples of the designed phase profile, the group delay (GD) profile, and the group delay dispersion (GDD) profile from top to bottom, respectively. Here, GD_{\min} and GD_{\max} are the minimum and maximum group delays, which are bounded by the meta-atom library. Figure 1B also highlights other key design parameters including phase discontinuity $\Delta\varnothing_i$, initial phase \varnothing_0 , and zone location r_i , which are inversely designed. We can increase the size of the metalens by increasing the zone number N , and we show simulation results of a 1-cm-diameter RGB-achromatic metalens (section S2). We can also apply this design principle to engineer light focusing at more than three colors by increasing the number of design frequencies in optimization.

The designed RGB-achromatic metalens with NA = 0.7 is composed of 681 zones using TiO_2 meta-atoms (21). Each individual zone is designed for achromatic focusing of the visible light ranging from 470 to 670 nm, and the group delay of meta-atoms in each zone is bounded by 2 and 4 fs. The phase discontinuities at zone boundaries are optimized to focus design wavelengths of 488, 532, and 658 nm at equal focal length. This metalens focuses incident light of left-handed circular polarization and converts it to right-handed circularly polarized light. The simulation of the intensity

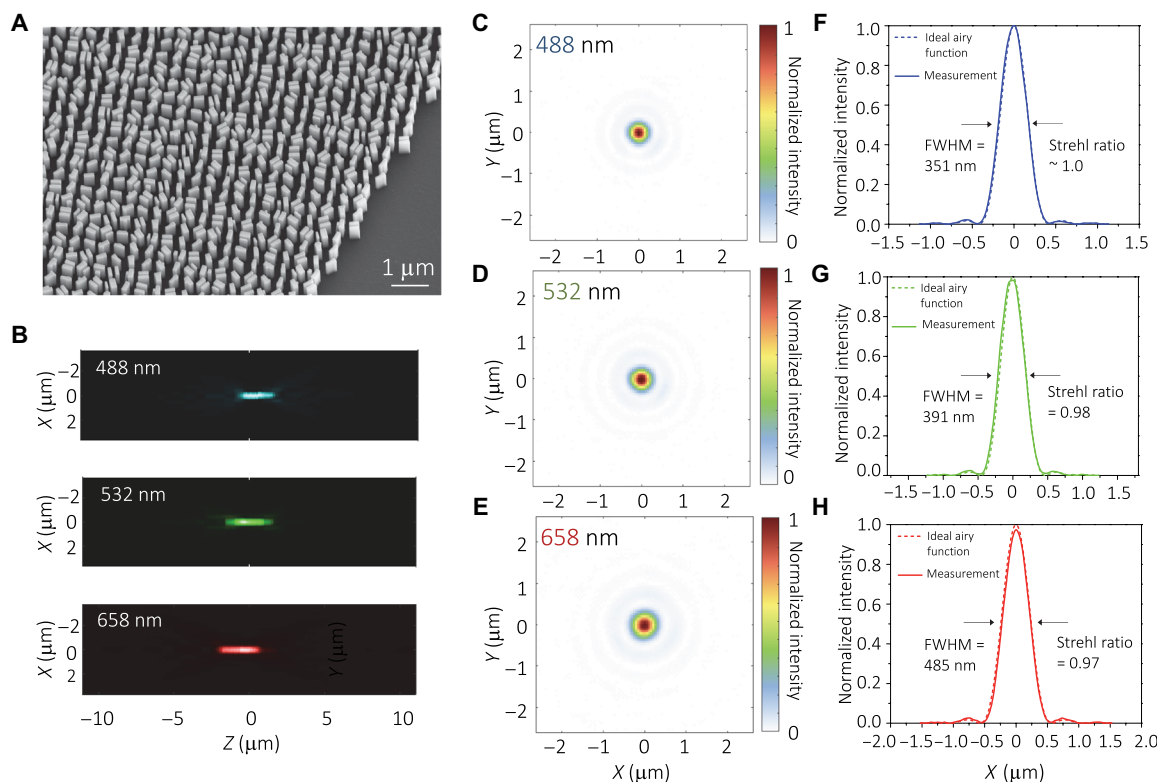


Fig. 2. Fabrication and characterizations of the RGB-achromatic metalens. (A) A scanning electron microscopic image of the fabricated metalens with NA = 0.7. Scale bar, 1 μm. (B) Measured focal intensity distribution of the metalens in the XZ plane showing negligible focal shift (~0.1% of the focal length) at the design wavelengths. (C to E) Measured focal intensity profiles in the focal planes. (F to H) Corresponding focusing intensity line profiles of (C) to (E). FWHM, full width at half maximum.

distribution at three wavelengths along the optical axis by using the Fresnel-Kirchhoff integral method (22) shows pronounced focusing peaks at the design focal length with negligible intensity elsewhere (Fig. 1D). The inset is the zoom-in view showing the same focal length at the design wavelengths. Figure 1 (E to G), shows the simulated intensity profiles of focal spots at three design wavelengths in the plane perpendicular to the optical axis (Z axis). The calculated Strehl ratios are all close to unity, indicating diffraction-limited focusing. For the metalens with $NA = 0.3$, we optimized not only the phase discontinuities at zone boundaries but also the zone transition locations and the RGB wavelengths. The optimization goals are maximizing the light intensity at the design focal spots and minimizing spurious focusing elsewhere along the optic axis (multifoci). Simulation results are summarized in section S3. The calculated Strehl ratios are also close to unity, and the intensity of spurious focal spots is greatly suppressed.

Focusing and imaging characterizations of the RGB-achromatic metalenses

Figure 2A shows a scanning electron microscope image of the fabricated 2-mm-diameter metalens with $NA = 0.7$ (see section S4 for additional images). The metalens is composed of TiO_2 nanofins of different geometries and rotation angles that are tailored for independent control of phases and dispersion. Figure 2B shows the measured focal intensity profile in the XZ plane of the metalens at the design wavelengths. The setup and measurement details are illustrated in section S3. The maximum focal shift among three focal spots at the RGB wavelengths is around $1 \mu\text{m}$, which is $\sim 0.1\%$ of the

design focal length. The error arises from fabrication imperfections. Figure 2 (C to E) shows the measured intensity distribution in the focal plane, and the corresponding Strehl ratios at the design wavelengths are all close to unity, as shown in Fig. 2 (F to H). Such nearly ideal focusing is the result of the combined effects of dispersion engineering and zone interference engineering. The RGB focusing of the metalens with $NA = 0.3$ is similarly achromatic and diffraction limited (section S3).

We characterized imaging of the metalens by using the USAF (United States Air Force) resolution target. For the metalens with $NA = 0.7$, we imaged elements no. 5 and no. 6 from group no. 7 using laser diodes with linewidths of $\sim 1 \text{ nm}$ (Fig. 3, A to C). The measurement setup is explained in detail in section S5. The smallest feature size is $\sim 2.2 \mu\text{m}$. The metalens not only resolves each bar but also captures the subtle imperfections of the bar edges. The slight blur is due to coma aberration. We also tested the imaging of this metalens in other synthesized colors by mixing two incident light sources (Fig. 3, D to F). Figure 3 (G and H) shows the imaging results under white light illumination synthesized by combining RGB laser diodes. We characterized the metalens with $NA = 0.3$ by imaging the whole group no. 7 of the resolution target. Here, we used a tunable supercontinuum laser (linewidth $> 5 \text{ nm}$) as a light source, and results are shown in Fig. 3 (I to K). Figure 3L shows the white light imaging result by combining RGB laser sources, and the imaging results of two-color mixing are summarized in section S5. The coma aberration of this metalens is less pronounced due to its smaller NA . We observed that imaging blur occurs when increasing light source linewidth (section S5).

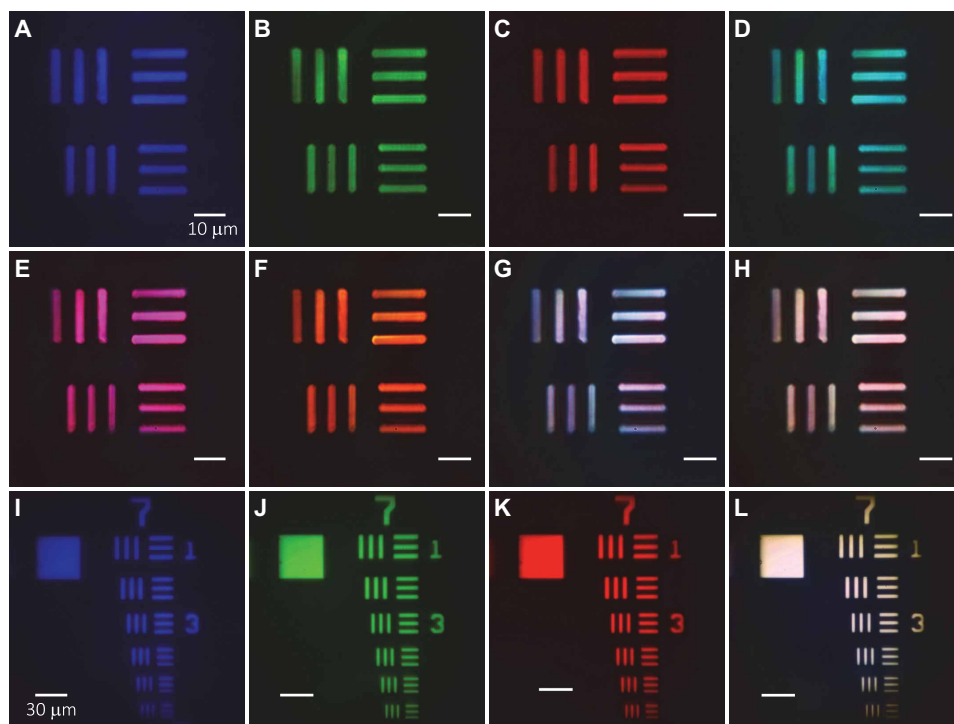


Fig. 3. Imaging of the USAF resolution target by the RGB-achromatic metalenses under different illumination. (A to C) Imaging results of the elements no. 5 and no. 6 from the group no. 7 of a USAF resolution target by the metalens with $NA = 0.7$ at design wavelengths of $\lambda = 488, 532,$ and 658 nm , respectively. The smallest line-width feature size is $2.2 \mu\text{m}$. Scale bars, $10 \mu\text{m}$. (D to F) Imaging results of the same target by the metalens of $NA = 0.7$ under synthesized light illumination by mixing two and (G and H) all three of the RGB laser sources. Scale bars, $10 \mu\text{m}$. (I to K) Imaging results of the whole group no. 7 of the USAF resolution target by the metalens with $NA = 0.3$ at design wavelengths of $\lambda = 470, 548,$ and 647 nm , respectively. Scale bars, $30 \mu\text{m}$ unless noted. (L) Imaging result of the target by the metalens under synthesized white light illumination that is composed of the RGB wavelengths.

Virtual and augmented reality demonstration

The diffraction-limited and RGB-achromatic focusing performances of our metalens are desirable for applications in compact image projection systems (23, 24), which have light emission centered at three discrete RGB wavelengths. Recent advances in VR technologies are hindered by eyepieces because of their bulky size (25, 26), heavy weight, and compromised viewing experience (27). Here, we demonstrated a VR platform on the basis of an RGB-achromatic metalens. The schematic of the VR system is shown in Fig. 4A (top).

An achromatic metalens is placed in front of an eyeball, and a display is placed within the focal plane of the metalens. The images shown on the display are magnified by the metalens, focused onto retina through eye lens crystal, and form virtual images appearing at far distance. In the experiment, we used a tube lens to mimic the eye lens crystal and a CMOS camera to mimic the retina. Figure 4A (bottom) is the cross-sectional view illustrating the VR system working principle. We show key design parameters of a VR device in section S6. The field of view (FOV) is determined by the NA of an

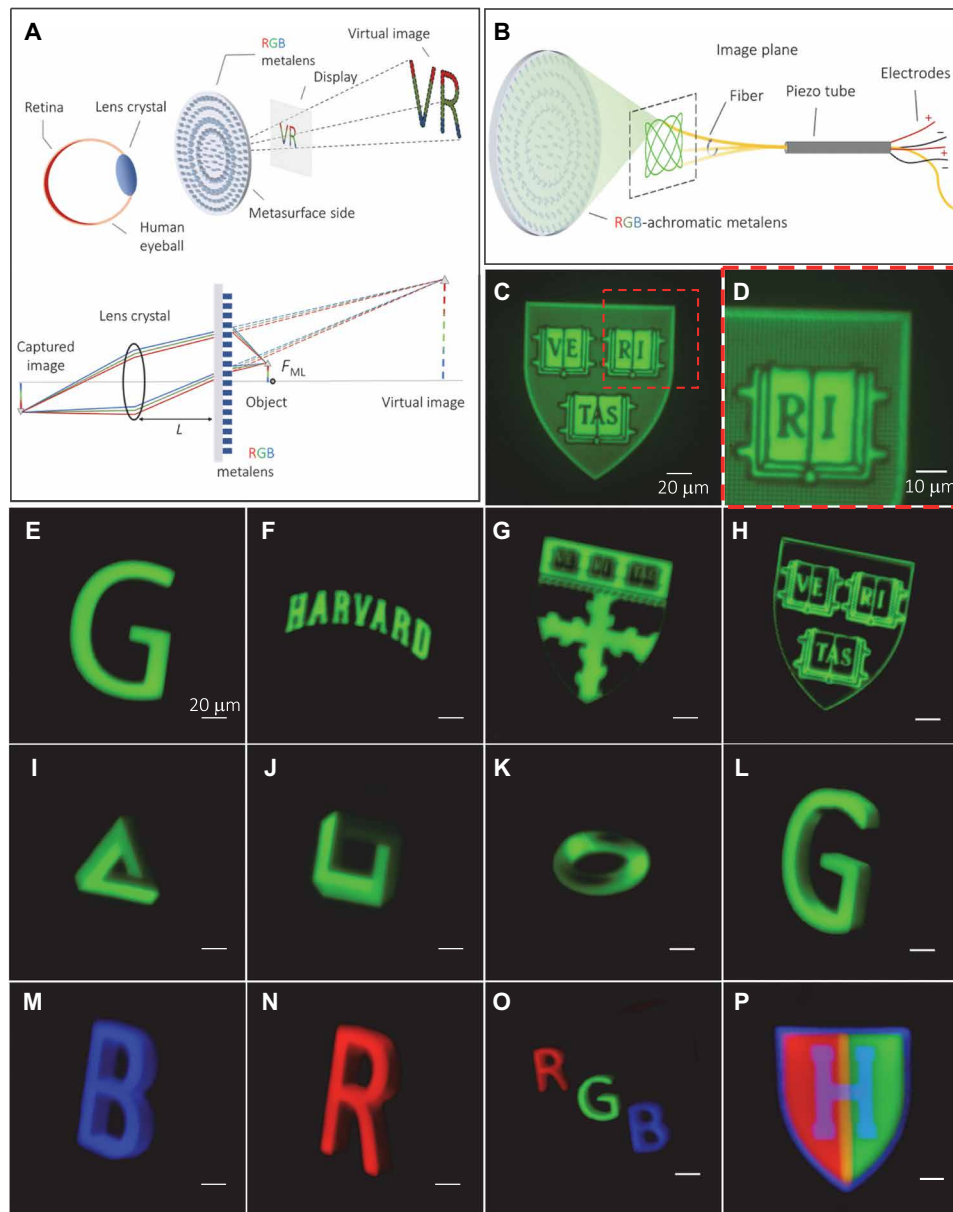


Fig. 4. VR demonstration. (A) Top: Schematic illustration of the VR mode. Bottom: Cross-section view illustrating its working principle. F_{ML} is the focal length of the metalens, and L (~ 7 cm) is the eye relief distance. (B) Schematic illustration of the near-eye fiber scanning display. (C) The VR imaging result using a passive display under the green light illumination at $\lambda = 548$ nm. Scale bar, 20 μm . (D) Zoomed-in view of (C). The dots inside the shield pattern, which mimic pixel grains, have a diameter of 1300 nm and can be clearly resolved (see fig. S21). Scale bar, 10 μm . (E to H) Four binary optical images captured in the VR mode at $\lambda = 548$ nm. The images are displayed by scanning the fiber tip in a Lissajous pattern and temporally modulating the incident light's intensity in two levels (on/off). Scale bars, 20 μm unless noted. (I to K) Virtual objects with a three-dimensional (3D) effect, which are displayed by applying multilevel intensity modulation. (L to N) VR images of G, B, and R letters with a 3D effect in three distinct colors by using continuous-level intensity modulation of incident light. (O) An RGB-color VR imaging result. (P) A VR image showing a "H" logo shield in seven colors, which are realized by mixing the primary RGB colors in space and time.

eyepiece; the form factor is determined by the size of the eyepiece and the display as well as by the distance between them. A desirable VR system should consist of a high-NA eyepiece and a miniaturized display. So far, most VR devices on the market are based on bulky refractive lenses, which suffer from not only chromatic aberrations but also low-NA focusing. For example, we characterized a lens from a commercial VR device (section S7). Meta-optics provides an alternative approach due to their combined merits.

Another challenge in current VR technologies is a desired near-eye display that offers combined advantages such as miniaturized footprint, high resolution, high dynamic range, high brightness, and wide color gamut. To achieve that, we first used a passive display that is mimicked by using patterned metal masks and laser beam illumination (section S8). We further developed a fiber scanning method for a near-eye display (28). Figure 4B depicts the schematic of a fiber scanning display. An optical fiber was mounted through a piezo actuator tube with the fiber tip positioned at distance L from the piezo. An electric signal was applied to the piezo actuator tube by two pairs of electrodes that were soldered onto the end of the tube. The applied voltage controls the movement of the fiber in two orthogonal directions and thus the trajectory of the fiber tip. The fiber tip scans in two dimensions and displays patterns when the incident light is guided through the optical fiber, thus forming a miniaturized display. To display arbitrary design patterns, light emission was modulated as a function of time in synchronization with the fiber tip movement (section S8). Fundamentally different from traditional liquid crystal display (LCD)/light-emitting diode (LED) displays where the pixel number is predefined by the single pixel size and the display size and the pixels are uniformly distributed in two-dimensional (2D) lattices, here, the pixel number of the fiber scanning display is determined by its light modulation speed, and the pixel distribution depends on its scanning method. We used and compared two scanning methods: Lissajous scanning and spiral scanning. The voltage signals applied onto the two electrodes are in the following form: $V_{x(y)}(t) = A_{x(y)}(t) \sin(2\pi f_{x(y)}t + \phi_{x(y)})$ where $A_{x(y)}$ is the voltage amplitude in $x(y)$ direction, $f_{x(y)}$ is the modulation frequency, and $\phi_{x(y)}$ is the initial phase. The details of our applied fiber scanning techniques are discussed in section S8. Figure 4C shows the VR imaging result using a passive display under green light illumination. Figure 4D is the zoomed-in view of Fig. 4C and shows clearly resolved dots inside the shield pattern that mimic pixels (section S8). The dots have a diameter of 1300 nm, which are smaller than the pixel sizes ($\sim 8 \mu\text{m}$) of current micro-LCD (micro-LED) display

on the market. Figure 4 (E to P) shows the VR imaging results using our home-built near-eye fiber scanning display. Figure 4 (E to H) shows four binary imaging examples consisting of 1 megapixel using green incident light in a VR demo. The fiber tip scans in a Lissajous pattern. The imaging results using red and blue incident light are shown in section S8. As can be seen from the virtual images captured by the camera, the light intensity distribution is quite uniform and the image resolution is reasonably high. The imaging results using the spiral scanning method are shown in section S8. Next, we demonstrated grayscale imaging that creates a 3D effect by applying a multilevel voltage to the acoustic-optic modulator. Figure 4 (I and J) shows a Penrose triangle image with four-level intensity and a Penrose square image with five-level intensity, respectively. A toroid image with a continuous intensity variation is also shown in Fig. 4K, which demonstrates the high dynamic range of the fiber scanning display. Figure 4 [L to N (three images)] shows grayscale images of RGB letters with 3D effects in distinct colors. We furthermore realized a full-color fiber scanning display by combining three different laser sources (section S8). Figure 4O shows a three-primary-color image displaying RGB letters in grayscale that is captured in VR mode. Figure 4P shows an H-letter-embodied shield logo in seven colors, of which three are primary RGB colors defined by the laser sources and the other four realized by color mixing. The RGB laser source linewidths are smaller than 5 nm, which infers wide color gamut (section S9). The footprint of the fiber scanning display could be reduced toward a portable device, and possible strategies are discussed in section S10. We compared the performance of our fiber scanning near-eye display with current existing display techniques on the market, and the results are summarized in section S9.

In addition, the RGB-achromatic metalens can be implemented into an augmented reality (AR) device, as shown in Fig. 5A. It allows the mixture of virtual objects and real-world scenes through an optical combiner (section S12). Figure 5B is the AR imaging result using the passive display. It shows that a virtual purple H-letter-embodied shield immerses in a real-world scene. Figure 5 (C and D) is the AR imaging result using the near-eye fiber scanning display, which shows floating virtual images of gadget icons and three-color RGB letters in a real-world scene, respectively (more information in section S12). Current challenges in VR/AR open new opportunities for dispersion-engineered metasurfaces, as discussed in section S13. For example, we designed a compact achromatic quarter wave plate on the basis of dispersion-engineered metasurfaces in simulation

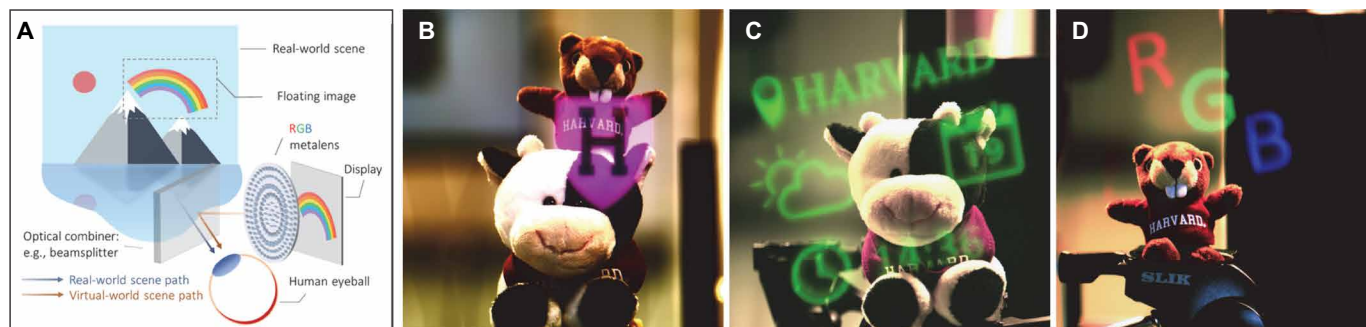


Fig. 5. AR demonstration. (A) Schematic illustration of the AR mode. (B) An AR image showing a floating H-shield logo pattern in purple color created by using a passive display immerses in a real-world scene. (C) An AR image showing the mixture of a real-world scene with a floating image that is created by the near-eye fiber scanning display. (D) The AR imaging result using the full-color near-eye fiber scanning display, which shows an RGB-color virtual image floating in a real-world scene. Photo credit: Zhaoyi Li, Harvard University.

and proposed a strategy to resolve eye's depth of cue by using a multi-focal RGB-achromatic metalens.

DISCUSSION

Further improvements are desirable for better implementation of a metalens in image projection applications. First, one challenge of a high-NA metalens is limited FOV. The metalens shown in this work corrects monochromatic aberrations and chromatic aberration for normal incidence. Its higher-order aberrations limit the VR device's FOV to be $<10^\circ$. We showed in simulation an RGB metalens doublet that can also correct coma aberration, field curvature, and transverse chromatic aberration for oblique incident beams for large FOV (section S14) (29, 30). Second, one can further increase the size of the metalens to centimeter scale and use the fabrication techniques that are feasible for large scale and mass production at low cost, such as deep UV (ultraviolet) stepper lithography (12, 31, 32), nanoimprint lithography (33), surface plasmon lithography (34), etc. Third, the focusing efficiency of the metalens can be improved by using multilayer unit cells and topological optimized meta-atoms in the future.

The co-engineering of dispersion and zone interference opens a new paradigm of metalens design, which represents a combination of forward and inverse design methods. We have demonstrated a path to a large yet thin lens that can simultaneously achieve diffraction-limited high-NA achromatic focusing at multiple wavelengths by engineering meta-atoms' dispersion and controlling constructive interference at every location. The meta-optics demonstrated in this work offer new paths to future VR/AR applications.

MATERIALS AND METHODS

Simulation

The metalens is composed of TiO_2 nanofin structures. The building block library was built up by using the rigorous coupled-wave analysis method and consisted of $\sim 60,000$ nanostructures with different geometries. The height of the TiO_2 nanofin is 600 nm and the periodicity of the unit cell is 400 nm. The incident light is set as a left-handed circularly polarized state, and the monitored transmitted light is in the conjugate right-handed circularly polarization state.

Fabrication

The metalens presented was fabricated on fused silica substrate in the following procedures: To begin with, the fused silica substrate was spun coated with a layer of 600-nm-thick positive electron beam resist (Zeon Chemicals, ZEP-520A), followed by an additional layer of conductive polymer (Showa Denko, ESPACER 300) to avoid charging effects during electron beam lithography. After that, the patterns were defined using electron beam lithography (Elionix, ELS-F125), and the exposed sample was then developed in *o*-xylene. Next, around 210-nm-thick amorphous TiO_2 was deposited directly onto the developed sample using atomic layer deposition (Cambridge Nanotech, Savannah). The TiO_2 not only filled in the trenches of the exposed e-beam resist but also coated on top of the unexposed sample area. We later removed the excess film of the TiO_2 by using reactive ion etching (Oxford Instrument, PlasmaPro 100 Cobra 300), and the etchant is a mixture of CHF_3 , O_2 , and Ar gas. Upon the completion of the etching processing, we stripped off the electron

beam resist by soaking the sample in Remover PG (MicroChem Corporation) for 24 hours.

SUPPLEMENTARY MATERIALS

Supplementary material for this article is available at <http://advances.sciencemag.org/cgi/content/full/7/5/eabe4458/DC1>

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